

Bioremediation Process of Effluent from Detergent and Food Industries in Jos, Nigeria: Kinetics and Thermodynamics

Akeem Adebayo Jimoh*¹, Dr Adebayo Ganiyu Babatunde², Dauda Baba³,
Abdullateef Baba⁴

¹Chemistry Department, College of Pure and Applied Sciences, Kwara State University, Malete. Ilorin, Nigeria.

²Industrial Chemistry Department, Faculty of Physical Sciences, University of Ilorin, Ilorin, Nigeria.

³Chemical Engineering Department, Faculty of Engineering, University of Maiduguri, Maiduguri, Nigeria.

⁴Chemistry Department, Faculty of Science, University of Maiduguri, Maiduguri, Nigeria.

Corresponding Author: Akeem Adebayo Jimoh

Abstract : In This Present Study, The Reduction Trends in Total Solids (TS) of Effluents from Food and Detergent Industries were used to determine the rate of Remediation using Immobilized Bacterial Substrates. Two different Bacteria *Pseudomonas Spp* and *Bacillus Spp* were isolated from Food Effluent (FE) and Detergent Effluents (DE) and were used for their remediation study. The results showed that the reduction in Total Solids (TS) ranged between 11.55% and 84.26% for Food Effluent and 17.89% and 97.84% for Detergent Effluent (DE) Respectively. The Reductions in TS were subjected to zero and first order kinetics. The rate constant for TS reduction for zero order kinetics were ranged (FE 0.095-0.758 Mg/L/Day and DE 0.036-1.029 Mg/L/Day) and first order kinetics also ranged (FE 0.015-0.238 D⁻¹ and DE 0.015-0.42 D⁻¹). The kinetic models' results showed that both the TS reduction for *Pseudomonas Spp.* and *Bacillus Spp.* used in this research followed both the zero order and first order kinetics.

Key Words: *Bacillus Spp.*, Immobilization, Kinetics, *Pseudomonas Spp.*, Thermodynamics.

Date of Submission: 27-02-2018

Date of acceptance: 14-03-2018

I. Introduction

Environmental bioremediation is an emerging technology which is receiving great attention because conventional methods to clean up the environment are cost-intensive and eco-unfriendly. Bioremediation is based on the idea that all organisms remove substances from the environment to carry out growth and metabolism [1]. Bioremediation make use of micro-organisms and higher plants to treat hazardous organic and metallic residues or by-products which enter into soils and sediments from various processes associated with domestic, municipal, agricultural, industrial and military activities [2].

A major concern for petroleum hydrocarbon bioremediation is the presence of heavy compounds such as polycyclic aromatic hydrocarbons (PAHs), asphaltenes and many branched compounds with 20 or more carbon atoms. These heavy hydrocarbon constituents are not easily metabolized by microorganisms and are considered potential health risks due to their possible carcinogenic and mutagenic actions [3]. Information on kinetics is extremely important because it describes the concentration of the chemical remaining at any time and permit prediction of the levels likely to be present at some future time [4].

Waters with high total dissolved solids (TDS) are unpalatable and potentially unhealthy. Water treatment plants use flocculants to aggregate suspended and dissolved solids into particles large enough to settle out of the water column in settling tanks. TDS on the other hand is equally important in water quality studies, though there was no serious health effect associated with TDS ingestion in water but some regulatory agencies recommended a maximum TDS value of 500 mg/l in drinking water supplies [5]- [6]. TDS concentration of 2200 mg/l in effluents has been reported by Jenkins [7] while Wesenberg [8] reported a value of 2700 mg/l. High TDS is one of the major sources of sediment which reduce the light penetration into water and ultimately decrease the photosynthesis. According to WHO [9], the palatability of water with TDS level of less than 600.00 mg/l is generally considered good; drinking water becomes significantly and increasingly unpalatable at TDS levels greater than about 1000.00 mg/l. Therefore, a guideline value of 1000.00 mg/l was established for TDS based on taste consideration [10].

Total Suspended Solids (TSS) include all the particles suspended in water which will not pass through a filter. Suspended solids are present in natural water [10], sanitary wastewater, and many types of industrial wastewaters. It is observed that a suspended solid absorb heat from sunlight, causing increase in water temperature and subsequently decreases level of dissolved oxygen. Some aquatic species are sensitive to

prolonged exposure to TSS and thus, monitoring of TSS is an important criterion for assessing the quality of water [11]. Total Solid (TS) comprises of total dissolved solids (TDS) and total suspended solids (TSS).

Investigation of bioremediation of diesel-contaminated using composting techniques was carried out. The results of applied first-order kinetics models agreed to a great extent with the experimental results [12]. The evaluation of microbial systems for bioremediation of petroleum refinery effluents in Nigeria was studied. The study revealed the high potency of the strains and the possibility of using them in bioremediation of petroleum refinery and petrochemical waste waters [13]. Heavy metal biosorption potential of *aspergillus* and *rhizopus* sp. isolated from wastewater treated soil was conducted. The findings revealed that fungi of metal polluted sites showed higher metal tolerance and bio-adsorption capacity of chromium and cadmium [14]. The kinetics of bioremediation of petroleum contaminated soil using a laboratory scale aerated reactor was studied. The results showed that the first order kinetic constants for the different bioreactors vary between 0.041 and 0.0071 / day [15]. Microbial degradation and its kinetics on crude oil polluted soil from Agbor area of the Niger Delta in Nigeria was worked on. A remediation efficiency of 81.69% was obtained on the sixth week indicating the efficiency and effectiveness of the process. The biodegradation process followed first order with a rate constant of 0.035 /day [16]. This research work aimed at studying the kinetics and thermodynamics of bioremediation process whereby the rate of biochemical reaction involving removal of TS from industrial effluent by microorganisms was studied for future reference.

II. Materials and Methods

2.1. Sampling Area and Collection of Samples

The Effluents was collected from two different production plants in a sterile 4 litres plastic container carried in an ice-chest and stored in a refrigerator before analysis. The sample was collected from the channel of flow into the river [17]. The concentration of TSS, TDS and TS were determined before and after the bioremediation.

2.2. Determination of Total Solids (TS)

A clean dish of suitable size was dried at 103-105°C in an oven to a constant weight. 100 ml of thoroughly mixed effluent sample was accurately pipette into a dish, weighed and evaporated to dryness on a steam bath. The residue was dried in an oven for about 1 hour at 103-105°C and re-weighed after cooling to room temperature. The cooling was done until the weight of the dish plus residue was constant to within 0.05 mg. the weight of the dish was subtracted to obtain the weight of the total solids [18] - [19]. This procedure was repeated for the biological treated sample of the effluent. The value of TS was calculated using the formula:

$$TS\left(\frac{mg}{l}\right) = \frac{\text{milligram of Total solid}}{\text{volume of sample}} \times 1000 \text{----- (1)}$$

2.3 Determination of Total Suspended Solids (TSS)

100 Ml of the sample of the effluent was withdrawn into a conical flask with a pipette. It was filtered with filter paper which was pre-dried at 103-105°C and weighed. The weight of the filter paper was subtracted from the weight of the filter paper containing the solids to obtain the weight of the suspended solids [18] - [19]. This procedure was repeated for the biological treated sample of the effluent. The value of TSS was calculated using the formula:

$$TSS\left(\frac{mg}{l}\right) = \frac{\text{milligram of Total solid}}{\text{volume of sample}} \times 1000 \text{----- (2)}$$

2.4 Determination of Total Dissolved Solids (TDS)

Dissolved Solids were obtained by difference between total solids and total suspended solids [18]- [19].

2.5. Isolation and Identification of Organisms

Dominant Organisms (Bacteria) were isolated using serial dilution [18]. The biochemical tests that were used to identified the bacteria were sulphate indole motility (sim), oxidase, catalase, phenylalanine deaminase (pd), indole, citrate, coagulase, methyl red (mr), nitrate reduction, voges-proskauer (vp), sugar and urease tests [20] - [21]

2.6. Immobilization of Organisms

Agar solution and inoculi was prepared separately. 50 ml of nutrient broth each of the inoculi was prepared in a mccartney bottles and incubated for 24 hours. A solution of agar-agar media was prepared by dissolving 10 g of the media powder in distilled water and made up to 500 ml mark in an erlenmeyer flask and was sterilized in an autoclave for 15 minutes and allowed to cool to 40-45°C [21]. The 4 ml of microorganism in nutrient broth was mixed with 36 ml of the prepared agar-agar media in petri-dish plates and then allowed to solidify. This was kept in the refrigerator for bioremediation and its kinetics studies.

2.7. Bioremediation of the Effluents

The solidified agar block was cut into cubes using a sterile knife; 0.1 ml phosphate buffer (pH 7.0) was added and kept in the refrigerator for 1 hour for curing. Phosphate buffer was decanted after 1 hour and the cubes were washed with sterile distilled water 3-4 times before it was used [22].

Two litres of the effluent was supplemented with minimum basal medium in g/l: Na (0.8), MgSO₄.7H₂O (0.001), KH₂PO₄ (2), NaNO₃ (2), CaCl₂.2H₂O (0.5) and NaHPO₄.12H₂O (2) and sterilized in an autoclave at 121°C for 15 minutes.

200 ml of the effluent was transferred into 250 ml conical flask. The content was covered with a cotton-wool ramped with foil paper to avoid contamination. A particular weight in grams (5 g, 10 g) each of immobilized microorganism cells was quickly transferred into the effluent in the conical flask in an inoculating chamber and agitated for five [23]. The concentrations of TSS, TDS and TS were determined daily for five days and the results used to monitor the kinetics of the bioremediation process.

2.8. Kinetic Study of the Bioremediation

In order to evaluate the kinetic studies of the bioremediation process, data was fitted into the zero-order and first-order models. The linear forms of zero-order and first-order kinetic equations are given in equations 3 and 4 respectively:

$$[C_t] = -kt + [C_o] \text{-----} (3)$$

$$\ln[C_t] = -kt + \ln[C_o] \text{-----} (4)$$

Where C_t represents the amount of parameters (TS) at time (daily) intervals t, C_o is the initial amount of parameters used at the beginning of the experiments and k_t represents the kinetic constants.

2.9. Thermodynamic Study of the Bioremediation

On the basis of the rate constants obtained from the temperature-dependent data of the rate of bioremediation, the thermodynamic parameters including ΔG, ΔH and ΔS could be estimated from Gibb's free energy equation: ΔG = ΔH – TΔS and gas equation: ΔG = –RTlnK_n by equating the two equations and solving the linear equation derived from its solution gave:

$$\ln K = -\frac{\Delta H}{R} \frac{1}{T} + \frac{\Delta S}{R}$$

$$y = mx + c$$

Where $-\frac{\Delta H}{R} = \text{slope}$, $\frac{\Delta S}{R} = \text{intercept}$ and R = gas constant

–ΔH = R × Slope And ΔS = R × Intercept

2.10. Statistical Analysis

The differences in the measured and experimental values of each parameter were carried out using SPSS software. The data were represented as mean ± standard deviation. All the data were analyzed statistically applying student 't' test, for all the studied parameters.

III. Results and Discussion

Table I: Physico-Chemical Properties of Samples before and after Bioremediation at 35°C.

Parameters	Sample FE		Sample DE		Tolerance Limits (USEPA, 1993; NESREA, 2007 And NAFDAC, 2000).		
	Before Treatment	After Treatment	Before Treatment	After Treatment	WHO	NESREA	NAFDAC
Odour	Offensive	Odourless	Pungent	Odourless	Odourless	Odourless	Odourless
Colour	Dirty Brown	Clear	Greenish Blue	Light Blue	Clear	Clear	Clear
pH	4.6	6.9	11.8	7.50	7.0-8.5	6-9	6.5-8.5
TSS(Mg/L)	0.052	0.608	0.694	0.081	500	500	500
TDS(Mg/L)	7.24	2.958	5.89	0.741	500	500	500
TS(Mg/L)	7.292	3.526	5.961	0.841	30	30	100.00

WHO: World Health Organisation, NESREA: National Environmental Standard and Regulatory Enforcement Agency, NAFDAC: National Agency for Foods and Drugs Administration Commission

Table II: Characterisation of Organisms in Effluent Samples.

	FS1*	DS1	FS2	DS2*	FS3	DS3	FS4	DS4
Shape	Irregular	Rhizoid	Circular	Circular	Circular	Circular	Rhizoid	Irregular
Elevation	Flat	Raised	Convex	Convex	Flat	Flat	Curve	Flat
Edge	Undulated	Rhizoid	Entire	Entire	Entire	Entire	Undulated	Undulated
Optical Characteristics	Opaque	Opaque	Opaque	Opaque	Transparent	Opaque	Opaque	Opaque
Pigmentation	Yellow	Light Yellow	Light Yellow	White	Yellow	Light Yellow	Light Yellow	Light Yellow
Colony Surface	Rough	Rough	Smooth	Smooth	Smooth	Smooth	Rough	Rough
Consistency	4/5	1/5	3/5	4/5	2/5	3/5	1/5	2/5

Table III: Biochemical Characteristics of Isolated Bacteria

BIOCHEMICAL TEST	DETERGENT SAMPLE	FOOD SAMPLE
MR Test	+	+
PD Test	-	-
VP Test	-	-
NaCl Test	+	+
Lysine Test	+	+
Indole Test	-	-
Nitrate Test	-	+
Urea Test	-	-
SIM Test	++	++
Glucose Test	Fermentive	Oxidative
Maltose Test	Fermentive	Oxidative
Catalase Test	+	+
Lactose Test	+	+
Oxidative	+	-
Citrate	+	+

+, ++ = Positive Result

- = Negative Result

Table IV: Bioremediation of undiluted sample of FE and DE at 35, 45, 55 and 65°C with 5.0g Agar-Agar.

Temp. (°C)	Time (Day)	TSS (Mg/L)		TDS (Mg/L)		TS (Mg/L)	
		FE	DE	FE	DE	FE	DE
35	1	0.088	0.144	5.678	4.600	5.766	4.744
	2	0.231	0.339	5.116	4.165	5.347	4.504
	3	0.453	0.621	4.737	2.705	5.183	3.326
	4	0.578	0.689	4.222	1.326	4.800	2.016
	5	0.608	0.694	2.958	0.787	3.526	0.841
45	1	0.067	0.081	6.812	5.20	6.879	5.281
	2	0.092	0.99	6.793	5.031	6.865	5.128
	3	0.124	0.128	6.621	4.966	6.745	5.094
	4	0.166	0.281	6.493	4.711	6.659	4.992
	5	0.181	0.313	6.266	4.584	6.450	4.897
55	1	0.294	0.128	6.241	5.115	6.355	5.243
	2	0.430	0.222	5.533	4.881	6.065	5.003
	3	0.684	0.297	4.844	4.443	5.528	4.740
	4	0.781	0.331	4.004	2.985	4.785	3.316
	5	0.863	0.403	2.439	2.042	3.205	2.446
65	1	0.0675	0.143	1.913	1.90	1.976	2.041
	2	0.167	0.520	1.190	1.011	1.357	1.877
	3	0.464	0.857	0.690	0.690	1.211	1.477
	4	0.833	1.056	0.350	0.478	1.183	1.334
	5	0.988	1.325	0.190	0.290	1.148	1.014

Table V: Bioremediation of 50% diluted sample of FE and DE at 35, 45, 55 and 65°C with 5.0g Agar-Agar.

Temp. (°C)	Time (Day)	TSS (Mg/L)		TDS (Mg/L)		TS (Mg/L)	
		FE	DE	FE	DE	FE	DE
35	1	0.052	0.081	3.792	2.537	3.844	2.418
	2	0.113	0.174	3.252	2.010	3.365	2.184
	3	0.186	0.236	2.555	1.570	2.741	1.806
	4	0.277	0.311	2.039	0.753	2.316	1.064
	5	0.304	0.376	1.609	0.083	1.913	0.459
45	1	0.031	0.049	3.890	3.455	3.921	3.504
	2	0.052	0.071	3.571	3.345	3.623	3.416
	3	0.096	0.095	3.336	2.853	3.017	2.522
	4	0.112	0.124	2.905	2.408	3.017	2.522
	5	0.135	0.156	2.656	1.960	2.791	2.116
55	1	0.149	0.097	2.998	2.414	3.147	2.511
	2	0.219	0.142	2.723	2.008	2.942	2.150
	3	0.361	0.196	2.195	1.785	2.556	1.981
	4	0.421	0.214	1.777	1.155	2.198	1.369
	5	0.453	0.256	1.352	0.670	1.805	0.926
65	1	0.028	0.068	1.232	1.316	1.260	1.384
	2	0.084	0.301	0.907	0.705	0.991	1.006
	3	0.302	0.439	0.404	0.402	0.706	0.841
	4	0.441	0.512	0.141	0.183	0.552	0.695
	5	0.462	0.618	0.051	0.028	0.512	0.646

Table VI: Bioremediation of undiluted sample of FE and DE at 35, 45, 55 and 65°C with 10g Agar-Agar.

Temp. (°C)	Time (Day)	TSS (Mg/L)		TDS (Mg/L)		TS (Mg/L)	
		FE	DE	FE	DE	FE	DE
35	1	0.166	0.193	3.785	4.736	3.951	4.949
	2	0.223	0.404	3.411	3.386	3.634	3.789
	3	0.394	0.725	2.842	1.183	3.236	1.908
	4	0.584	0.804	2.621	0.824	3.192	1.628
	5	0.633	0.926	1.972	0.314	2.605	1.240
45	1	0.152	0.196	4.541	5.024	4.693	5.220
	2	0.196	0.262	4.234	4.484	4.430	4.746
	3	0.247	0.342	4.102	3.932	4.249	4.294
	4	0.315	0.399	3.962	3.557	4.277	3.956
	5	0.306	0.462	3.884	3.162	4.290	3.624
55	1	0.314	0.223	4.339	4.962	4.851	5.185
	2	0.396	0.385	4.165	3.524	4.761	3.909
	3	0.769	0.436	3.822	3.124	4.589	3.56
	4	0.384	0.569	3.229	2.143	4.113	2.712
	5	1.002	0.702	2.964	1.524	3.966	2.226
65	1	0.123	0.735	1.624	1.974	1.717	2.359
	2	0.256	0.684	1.468	1.648	1.724	2.332
	3	0.633	0.983	0.942	1.335	1.575	2.318
	4	0.964	1.174	0.423	1.084	1.387	2.20
	5	1.129	1.492	0.158	0.724	1.287	2.216

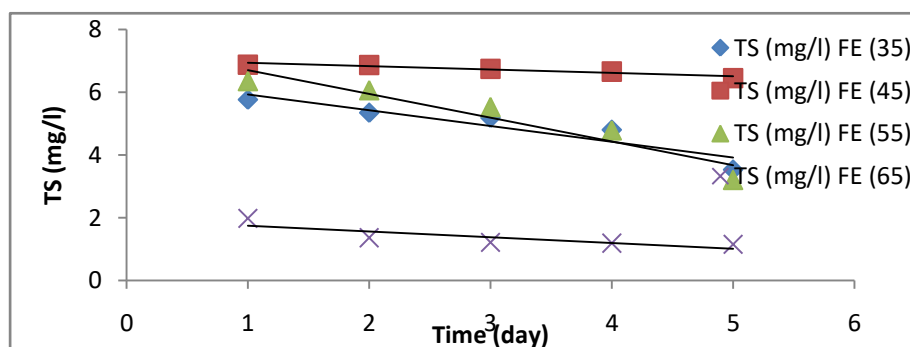


Figure 1: Graph of zero-order kinetics of TS against time at different temperature (undiluted sample FE with 5g Immobilized Bacteria)

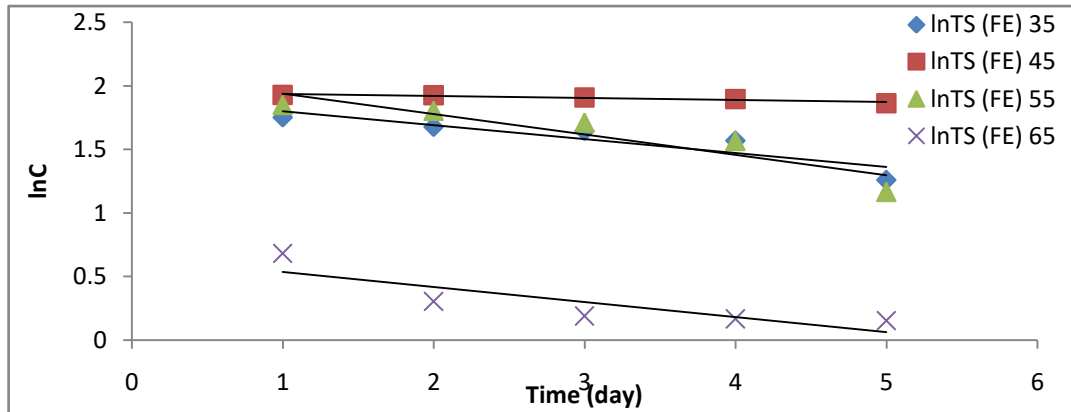


Figure 2: Graph of first-order kinetics of TS against time at different temperature (undiluted sample FE with 5g Immobilized Bacteria)

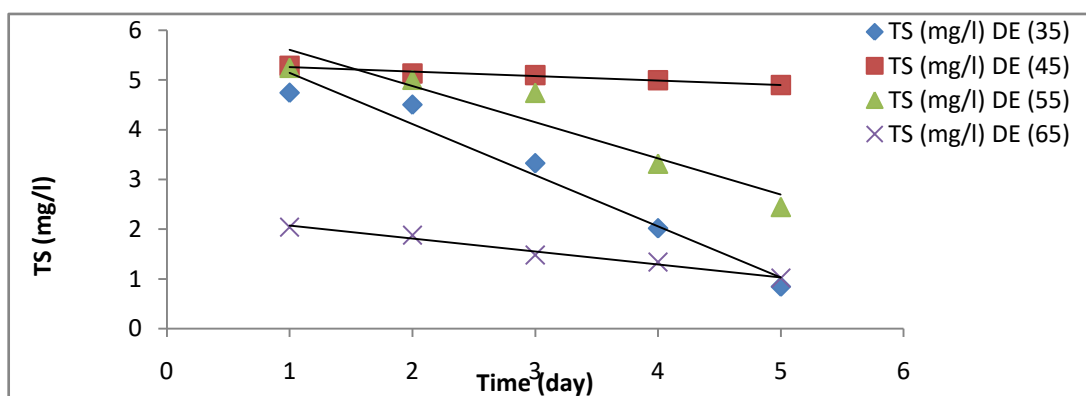


Figure 3: Graph of zero-order kinetics of TS against time at different temperature (undiluted sample DE with 5g Immobilized Bacteria)

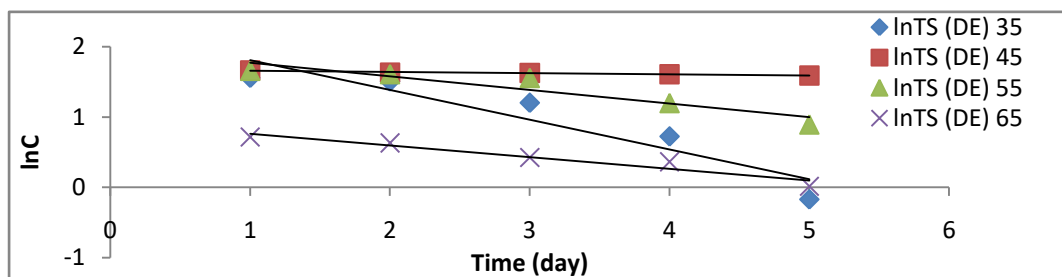


Figure 4: Graph of first-order kinetics of TS against time at different temperature (undiluted sample DE with 5g Immobilized Bacteria)

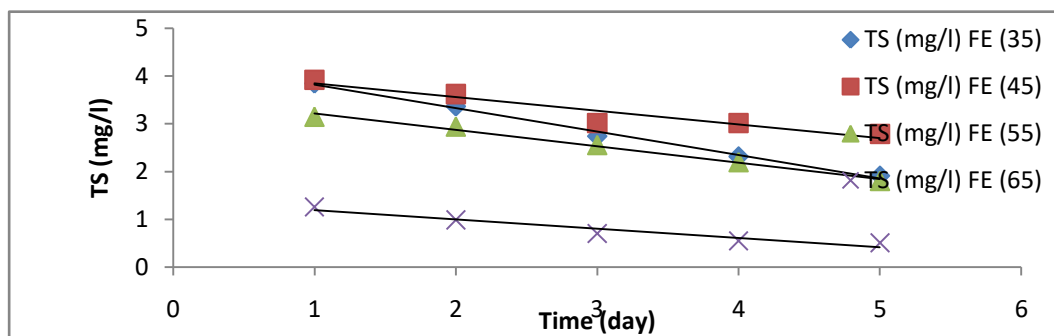


Figure 5: Graph of zero-order kinetics of TS against time at different temperature (diluted sample FE with 5g Immobilized Bacteria)

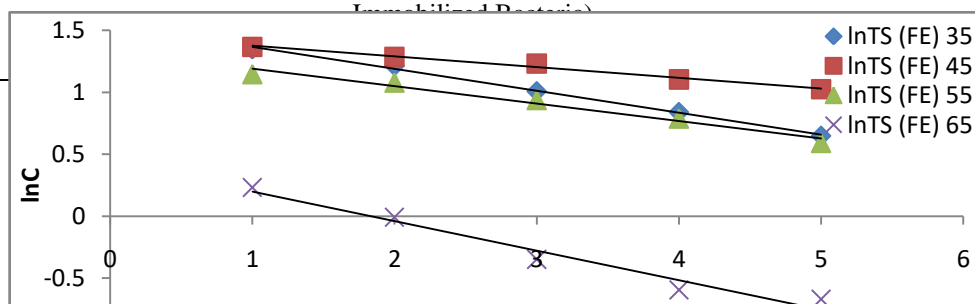


Figure 6: Graph of first-order kinetics of TS against time at different temperature (diluted sample FE with 5g Immobilized Bacteria)

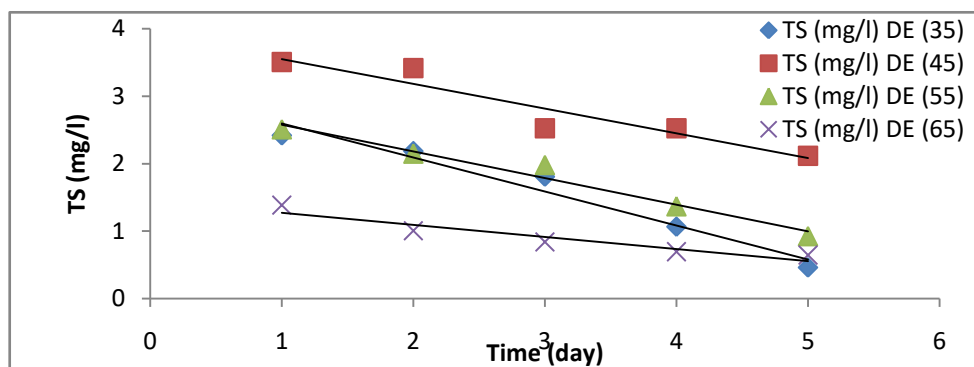


Figure 7: Graph of zero-order kinetics of TS against time at different temperature (diluted sample DE with 5g Immobilized Bacteria)

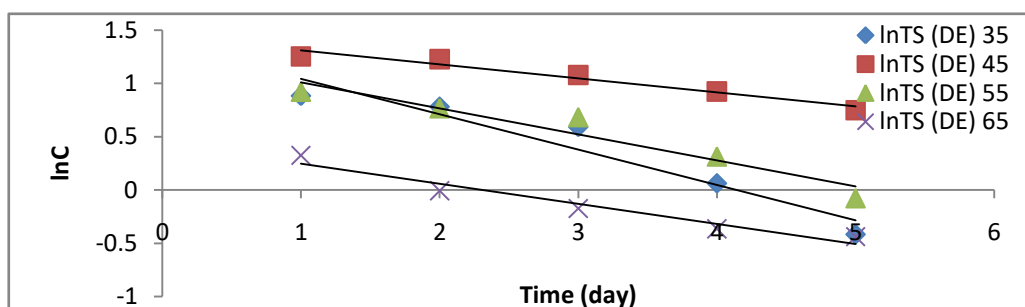


Figure 8: Graph of first-order kinetics of TS against time at different temperature (diluted sample DE with 5g Immobilized Bacteria)

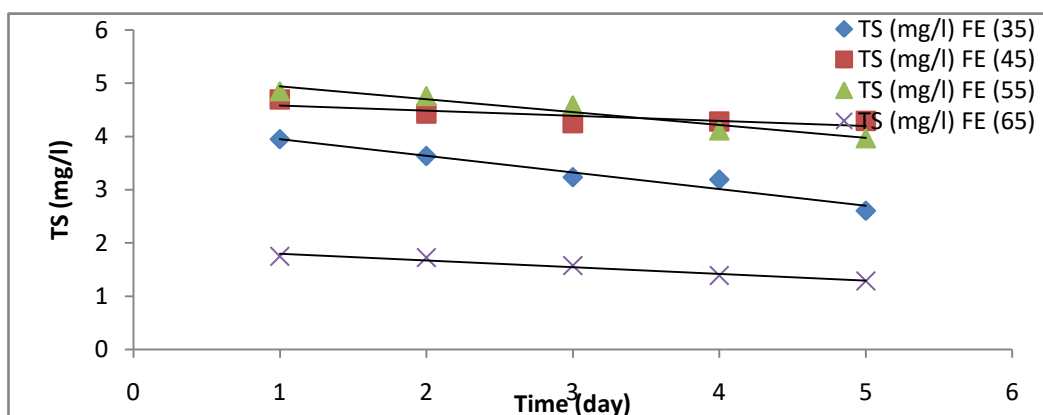


Figure 9: Graph of zero-order kinetics of TS against time at different temperature (undiluted sample FE with 10g Immobilized Bacteria)

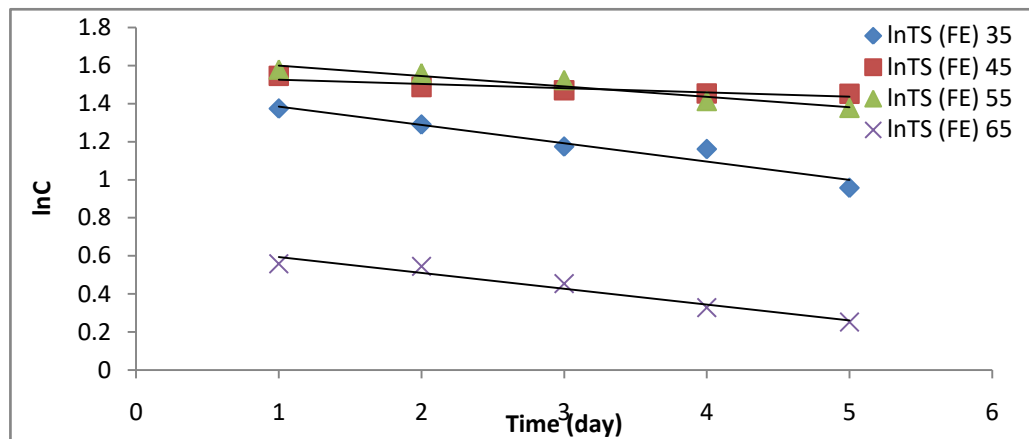


Figure 10: Graph of first-order kinetics of TS against time at different temperature (undiluted sample FE with 10g Immobilized Bacteria)

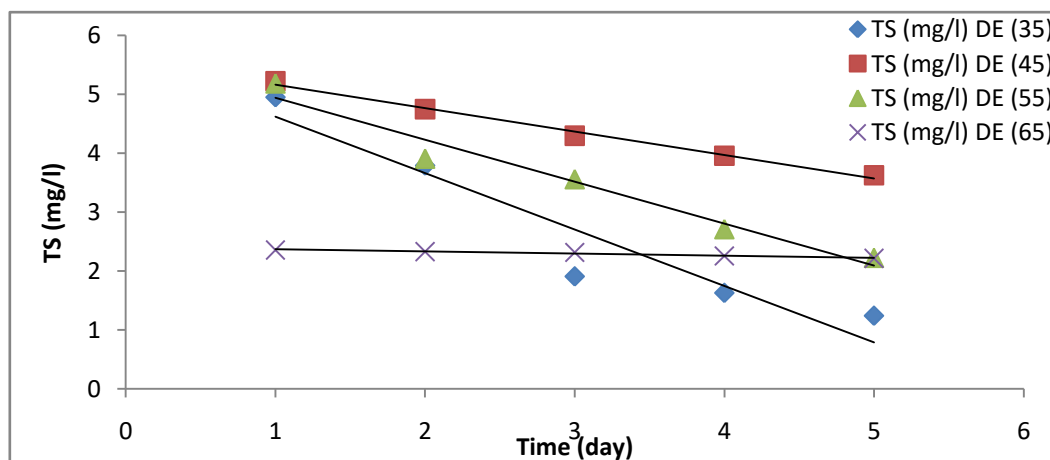


Figure 11: Graph of zero-order kinetics of TS against time at different temperature (undiluted sample DE with 10g Immobilized Bacteria)

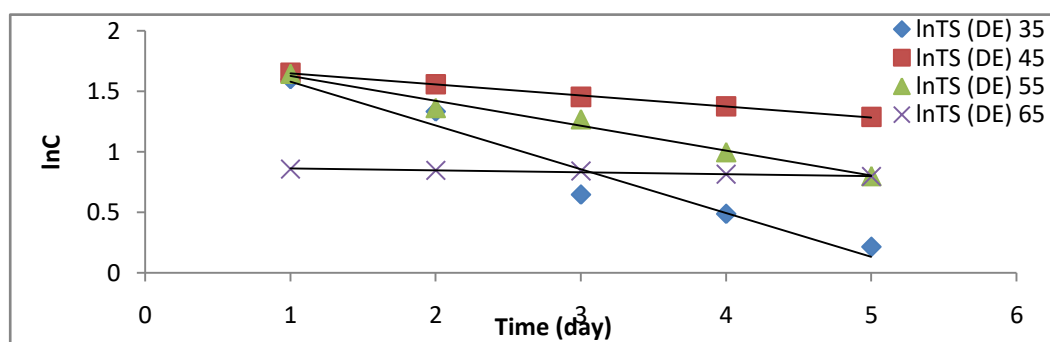


Figure 12: Graph of first-order kinetics of TS against time at different temperature (undiluted sample DE with 10g Immobilized Bacteria)

Table VII: Data for Thermodynamics parameters for TS in both samples

Temp.(T) (K)	Quantity Ads. (C _e) Mg/L		Quantity Rem. (C _a) Mg/L		C _a / C _e =K		Lnk		1/T (1/K)
	FE	DE	FE	DE	FE	DE	FE	DE	
308	3.766	5.120	3.526	0.841	1.068	6.08SS8	0.066	1.806	0.00325
318	0.842	1.064	6.450	4.897	0.131	0.217	-2.036	-1.527	0.00315
328	4.387	3.515	2.905	2.445	1.510	1.438	0.412	0.363	0.00305
338	6.144	4.347	1.148	1.614	5.352	2.693	1.678	0.991	0.00296

Table 8: Data for Thermodynamics ΔH , ΔS and ΔG for both samples using TS.

ΔH (Kj/Mol)		ΔS (Kj/Molk)		ΔG (Kj/Mol)							
				308K		318K		328K		338K	
FE	DE	FE	DE	FE	DE	FE	DE	FE	DE	FE	DE
+118.09	+162.12	+0.36	+0.50	+8.34	+9.78	+4.15	+4.83	+0.56	-0.11	-3.02	-5.06

3.1 Physico-Chemical Parameters

The Physico-Chemical parameters of the two effluents were summarised as shown in the table 1. The dirty brown colour and offensive odour of FE could be attributed to the decayed food raw materials and leftover substances which may likely be heavy metallic ions like iron (ii) and copper (ii) materials which were likely used during the production process while the pungent smell and greenish blue colour of DE could be due to the presence of sulphates of heavy metals like iron and copper used for production of detergent. The pH of both samples was found to range between acidic and alkaline region. It was acidic in sample FE and strongly alkaline in DE. The strong alkalinity is expected as the effluents were from detergent industry while acidity in FE could be attributed to the precipitation of additives used which may be metals during production. It has been reported that the solubility of metal hydroxides are enhanced by lowering the pH [24]-[25]. The pH of both samples at 35°C were far from the recommended standard limits of regulating bodies WHO (7.0-8.5), NESREA (6-9) and NAFDAC (6.5-8.5). While FE fell within the acidic range of 4.6, DE fell within the alkaline range of 11.8. However, at the end of the biological treatment, both samples were being remediated to 6.9 and 7.5 respectively.

The TSS, TDS, and TS values obtained could be attributed to oxidation products of the by-products of food materials and also the presence of the hydroxides of heavy metals mentioned earlier. However, the values obtained before treatment fell below the recommended standard limit of all the regulating bodies. This is an indication that the effluents were likely to have been treated before discharging into the effluent reservoirs.

3.2 Isolation and Identification of Bacteria

It was found that four organisms were able to grow on each effluent samples (table 2). The most repeating and predominant organism (FS1* And DS2*) in each samples were separately cultivated, and a pure culture was incubated in each case. The results of identification of isolated bacteria using biochemical tests and partial sequence of gene are shown in table 3 and table 4. Two universal oligonucleotides were used to determine and identify the gene for the two isolates which were the predominant organisms from respective isolations of food and detergent effluents. The results were confirmed with biochemical tests and showed that organism from samples FE and DE were *pseudomonas aeruginosa* strain 1242 and *bacillus subtilis* strain bl 10 respectively. These results were confirmed by comparing with the work reported by moslem et al [26].

3.3 Reduction of TS at 35°C, 45°C, 55°C and 65°C

Table 4 shows the trends in increment of TSS, TDS and TS at 35°C, 45°C, 55°C and 65°C for undiluted samples of DE and FE with 5 g immobilized bacteria. The TS of the two samples reduces by 51.65% and 85.89% for FE and DE respectively. It is evident that the rate of removal of contaminants was rather slow at temperature of 45°C. It is believed that the microorganisms (both *pseudomonas* spp. and *bacillus* spp.) were inactive at this temperature, i.e. they have gone into recession, although they were able to feed and remove some of the contaminant but at a slower rate. The results show that the percentage formation of TS 11.55% and 17.89% of FE and DE samples respectively as compared to 51.65% and 85.89.77% at 35°C were slow down due to the inactivity of the organism. This observation indicated that the influence of temperature is very important in the process of bioremediation as it affects the microorganisms when it is high by rendering them inactive or even killing them. However, there was an increase in rate of bioremediation as the temperature was increased to 55°C and 65°C respectively. This could be attributed to the fact that microorganisms particularly the mesophiles (category which both *pseudomonas aeruginosa* and *bacillus subtilis* fall) would not survive any temperature above 45°C indicating that at temperature (55°C and 65°C) the organism were expected to have been killed. However, dead microbial biomasses, including fungal mycelium have been reported to also adsorb contaminants, often in larger quantities than living biomass [27]. Moreover, immobilisation of the organisms was a factor that may cause increase in their efficiency. Enzymes often are able to work in multiple environments especially if they are immobilized. This makes the microorganisms' enzymes even more resistant to harsh environments and enables the enzymes to be recovered and recycled after they are no longer needed [28]. In general; immobilization makes the enzyme more resistant to temperature, pH and substrate concentration swings giving it a longer lifetime and higher productivity per active unit [28]-[31]. The results show further increase in bioremediation at 55°C as the removal of TS (56.05% and 58.97% of FE and DE samples respectively). The removal of TS is 84.26% and 82.99% from FE and DE samples respectively. It could however be summarise that temperature was the determinant factor for achieving high efficiencies of bioremediation processes [2].

Table 5 shows the trends of results of bioremediation of 50% diluted samples of FE and DE with 5.0 g of immobilized microorganism in agar-agar media. The results show that there is a similar trend for TS when compared with the results for the undiluted sample. It was observed that the dilution of the effluents caused reduction in the concentration of the contaminants. This reduction in the initial concentration of the contaminants made the rate of bioremediation to be faster as compared with those of original effluents. Diluting the samples indicated that the levels of contaminants were reduced due to interaction with water. there was reduction in the values of TS.

Table 6 shows the trends of results of bioremediation of undiluted sample with 10 g immobilized microorganism. The results show that there is a similar trend in TS when compared to those results in table 4. The TS were decreasing at each interval. The value of TS of FE and DE samples reduced at a percentage of 64.28% and 79.20% respectively.

3.4 Kinetics Study

Figures 1 To 4 show the graphs of zero-order and first-order kinetics of undiluted samples of FE and DE with 5 g immobilized bacteria. The TS reduction was studied at different temperatures and it was subjected to kinetic modelling. For the zeroth-order, the results showed that the rate constants varied between 0.106-0.758 mg/l/day and 0.258-1.029 mg/l/day for sample FE and DE respectively. The correlation coefficient of the plots showed that bioreaction at 45°C (0.906) and 55°C (0.916) were above 0.9 for sample FE while all the plots for sample DE have correlation coefficient greater than 0.9 with the highest at 45°C (0.981). also, the experimental values at 45°C (7.038 mg/l) and 55°C (7.461 mg/l) are more closer to the measured value 7.292 mg/l for sample FE while the experimental value of 5.344 mg/l at 45°C was more closer to measured value of 5.961 mg/l for sample DE. The difference between the measured and experimental values of zero order for both samples were insignificant ($p > 0.05$).

However, the first-order kinetic study showed that rate constants varied between 0.015-0.16 D⁻¹ and 0.017-0.42 D⁻¹ with the highest values in both samples FE and DE at 35°C. The correlation coefficients values at 35°C, 55°C and 65°C were all lower than 0.9 in both samples, while at 45°C of samples FE and DE the value was 0.908 and 0.963 respectively were above 0.9. The experimental value of sample FE at 45°C (7.043 Mg/L) was only value closer to the measured value 7.292 Mg/L while sample DE also at 45°C (5.344) was closer to the measured value 5.961 Mg/L. The difference between the measured and experimental values of first order for both samples were insignificant ($P > 0.05$).

The kinetic modelling of TS for sample FE using 5g Immobilised Bacteria showed that at 35°C, 45°C and 55°C zero order model was better fitted, having higher correlation coefficient as compared to its zero order. At 65°C it was first order that was better fitted. Meanwhile, sample DE was zero order at all temperature used.

Figures 5 To 8 show the graphs of zero-order and first-order kinetics of DILUTED SAMPLES of FE and DE with 5 g Immobilized Bacteria. The effect of dilution on the rate of removal of TS was studied. The zero order rate constants of TS reduction of diluted effluent samples varied between 0.193-0.491 Mg/L/Day and 0.178-0.503 Mg/L/Day for sample FE and DE Respectively. The highest value was at 35°C in both samples. The correlation coefficients of both samples were greater than 0.90, the highest value for sample FE was 0.993 at 35°C, while that of sample DE was 0.955 at 45°C. The intercept of the plots showed that experimental values of sample FE at 35°C (4.309 Mg/L) was close to the measured value (4.363 Mg/L) and that of sample DE at 45°C (3.917 Mg/L) was also close to the measured value (3.907 Mg/L). The difference between the measured and experimental values for zero order kinetics of both sample were insignificant ($P > 0.05$). This show that the zero-order modelling of TS reduction is better fitted at 35°C for sample FE and 45°C for sample DE.

Meanwhile, the first-order kinetic shows that the rate constants of samples FE and DE varied between 0.086-0.238 D⁻¹ and 0.131-0.331 D⁻¹ respectively. The correlation coefficients of the plots have values greater than 0.9 in both samples. The highest in each case were 0.996 at 35°C for sample FE and 0.955 at 45°C for sample DE. The experimental values of sample FE at 45°C and 35°C (4.315 And 4.674 Mg/L) were both close to the measured value 4.363 Mg/L, while that of sample DE also at 35°C AND 45°C (3.955 and 4.225 Mg/L) compared well with the measured value of 3.903 Mg/L. The difference between the measured and experimental values of first order kinetics for both sample were insignificant ($P > 0.05$).

At 50% dilution of the samples, the TS kinetic modeling for sample FE showed that first order model was better fitted at 35°C, 45°C and 65°C but at 55°C zero order models was better fitted. However, those of sample DE were better fitted at 35°C and 65°C with zero order models but at 45°C and 55°C the first order model were better fitted.

Figures 9 To 12 show the graphs of zero-order and first-order kinetics of undiluted samples of FE and DE with 10 g immobilized bacteria respectively. The rate constants of the zero-order kinetic were determined; and were ranged between 0.095-0.313 Mg/L/Day and 0.036-0.957 Mg/L/Day for samples FE and DE respectively. The highest value in each sample was at 35°C. The correlation coefficients varied between 0.676-

0.957 and 0.903-0.992 for sample FE and DE respectively; the highest was at 35°C for sample FE and 45°C for sample DE. None of the experimental values of sample FE were close to the measured value but sample DE at 35°C (5.576), 45°C (5.562) and 55°C (5.652) were all close to the measured value of 5.961 Mg/L. The statistical t-test analysis showed that the difference between the measured and experimental values of zero order kinetics for sample FE were significant ($P < 0.05$) while those of sample DE were insignificant ($P > 0.05$).

However, the rate constants of the first-order kinetic study were ranged between 0.022-0.096 D^{-1} and 0.015-0.361 D^{-1} for samples FE and DE respectively; the highest rate constant in both samples was at 35°C. This indicates that living organism perform better at room temperature. The correlation coefficients at 35°C 0.934 and 65°C 0.951 have higher values for sample FE while those of sample DE were higher than 0.95. The experimental values of the plots for sample FE at all temperatures were not comparable with the measured value. But those of sample DE at 45°C (5.692 Mg/L) and 55°C (6.246) were close to the measured value 5.961 Mg/L. The statistical t-test analysis showed that showed that the difference between the measured and experimental values of first order kinetics for sample FE were significant ($P < 0.05$) DE were insignificant ($P > 0.05$).

Using 10 g of immobilised biomass, the kinetic modelling of TS removal indicated that at 35°C, 55°C and 65°C zero order models had higher correlation as compared to those of its corresponding values from the first order models. At 45°C the first order model was better fitted. However, sample DE had better kinetic model as first order at 35°C, 45°C and 55°C but zero order model was better fitted at 65°C.

3.5 Thermodynamics Study

The effect of temperature on bioremediation process leads to the study of its thermodynamic as it is essential to know the spontaneity of the removal of various contaminants in both effluents. The Values of the entropy change (ΔS) and enthalpy (ΔH) were positive and large for both samples which signify chemisorptions. It could be observed that ΔH was all positive for all systems which confirmed favorability of the processes. It has been observed that the heat evolved during physisorption generally lies in the range of 2.1-20.9 $KJmol^{-1}$, while the heat of chemisorption falls into a range of 80-200 $KJmol^{-1}$ [32]. This indicated that the bioreaction is endothermic but the feasibility of the removal of TS were very small at temperature region from 308 to 318K because the Gibb's Free Energy (ΔG) were positive in both samples. The positive values of ΔS are an indication of an increased disorderliness and randomness at the bacteria-solution interface. ΔG decreases in magnitude from +8.981 to -8.064 KJ/Mol for temperature range from 308 to 338K. At a higher temperature of 328 and 338K, the bioreaction became feasible and spontaneous as the ΔG values changed to negative. The ΔG values which were all positive decreased with increasing in temperature. Although, the process was not spontaneous, it can be improved upon by increasing the temperature. This is in agreement with the result presented in the similar work of Omar and Al-Itaw [33].

IV. Conclusion

The following conclusions were made from the results and the discussion:

- i. The result revealed that the values of TS in both effluent samples FE and DE were lower than the standard tolerance limits.
- ii. The characterisation and biochemical tests of the isolated organisms revealed that the most active organisms were *Pseudomonas Aeruginosa* in sample FE and *Bacillus Subtilis* in sample DE.
- iii. The bioremediation of Food and Detergent Effluents by *Pseudomonas Aeruginosa* and *Bacillus Subtilis* respectively showed a significant reduction of the TS level in the effluents making the effluents safe for discharge into environment.
- iv. Biological treatment of these effluents was carried out at different time intervals in order to study the rate of bioremediation. Data obtained at each interval were subjected to zero and first order kinetic models. The results revealed that both models were well fitted for bioremediation process but first-order kinetic model provide a better approximation for the rate of removal of TS.
- v. The results obtained from the rate experiment were used to study the thermodynamics of bioremediation process. It was found that the process was faster as the temperature was increasing; revealing that temperature is a very important factor of bioremediation. The removals of TS were endothermic i.e. positive enthalpy change and thermodynamically stable since increase in temperature increases the spontaneity of bioremediation process.

References

- [1]. E. J. Bouwer and A. J. B. Zehnder, Bioremediation of Organic Compounds—Putting Microbial Metabolism to work, *Trends Biotech*, 11(8), 1993, 360-367.
- [2]. S. Ranenand C. Sharadinadra, Biotechnology Applications to Environmental Remediation in Resource Exploitation, *Current Science*, 97, 2009, 6-25.
- [3]. H. Baheri, and P. Meysami, Feasibility of Fungi Bioaugmentation in Composting a Flare Pit Soil, *Journal of Hazardous Materials*, 89, 2002, 279–286.
- [4]. M. S. Bruines, S. Kafil, and F. W. Oehme, Microbial Resistance to Metals in the Environment, *Ecotoxicology Environmental Safety Environmental Research*, 45, 2000, 198-207.
- [5]. FEPA. "Guidelines and Standards for Environmental Pollution Control in Nigeria". Federal Environmental Protection Agency Nigeria. 1991.
- [6]. NAFDAC. (National Agency for Food and Drug Administration and Control) *Commission Consumer Bulletin*, 2001. 1, 9.
- [7]. R. Jankins, *Pretreatment of Textile Waste Water*, Proc. 37th Industrial Waste Conference Purdue Uni. Lafayette, Ind. 1982, 37-139
- [8]. D. Wesenberg, I. Kyriakides, and S. N. Agathos, White-Rot Fungi and Their Enzymes for the Treatment of Industrial Dye Effluents, *Journal of Biotechnology Advance*, 22, 2003, 161-187.
- [9]. WHO, *Air Quality Guidelines* (World Health Organization, Europe Regional Office, Copenhagen, 2006
- [10]. WHO, *Water Treatment and Pathogen Control: Process Efficiency in Achieving Safe Drinking Water* (IWA Publication, UK, 2004, Pp. 1890)
- [11]. J. C. Akan, V. O. Ogugbuaja, F. I. Abdulrahman, and J. T. Ayodele, Pollutant Levels in Effluent Samples from Tanneries and Textiles of Kano industrial areas, Nigeria, *Global Journal of Pure and Applied Sciences*, 15(3), 2009, 343-352
- [12]. E. Hwang, W. Namkoog, and J. Park, Recycling of Remediated Soil for Effective Composting of Diesel- Contaminated Soil, *Compost Science and Utilization*, 2001, 143-149.
- [13]. T. V. Ojumu, O. O. Bello, J. A. Sonibare, and B. O. Solomon, Evaluation of Microbial Systems for Bioremediation of Petroleum Refinery Effluents in Nigeria, *African Journal of Biotechnology*, 4(1), 2005, 31-35.
- [14]. A. Iqbal, Z. Shaheen, and A. Farah, Heavy Metal Biosorption Potential of *Aspergillus* and *Rhizopus* Sp. Isolated from Wastewater Treated Soil, *J. Appl. Sci. Environ Mgt*, 9 (1), 2005, 123–126.
- [15]. E. A. Bassim, and D. S. Walid, Kinetics of Indigenous Isolated Bacteria used for Ex-Situ Bioremediation of Petroleum Contaminated Soil, *Water Air Soil Pollution*, 192, 2008, 221-226
- [16]. O. V. Akpoveta, F. Egharevba, and O. W. Medjor, A Pilot Study on the Biodegradation of Hydrocarbon and its Kinetics on Kerosene Simulated Soil, *International Journal of Environmental Science*, 2(1), 2011.
- [17]. G. B. Adebayo, G. A. Otunola, and T. A. Ajao, Assessment and Biological Treatment of Effluent from Textile Industry, *African Journal of Biotechnology*, 9(49), 2010, 8365- 8368.
- [18]. APHA. *Standard Methods for Examination of Waste and Wastewater* (15th Edition. Brydpass Springfield, Washington DC, 1989) 164-176.
- [19]. C. M. Ademoroti, *A Standard Methods for Water and Effluent Analysis* (1st Edition, 1996) 20-50.
- [20]. Fawole, M. O.; Oso, B. A. *Laboratory Manual of Municipal of Microbiology*. Spectrum Books Limited, 1988.
- [21]. A. T. Ajao, G. B. Adebayo and S. E. Yakubu, Bioremediation of Textile Industrial Effluent Using Mixed Culture of *Pseudomonas Aeruginosa* and *Bacillus Subtilis* Immobilized on Agar-Agar in a Bioreactor *J. Microbiol. Biotech. Res.* 1(3), 2011, 50-56
- [22]. P. Ellaiah, K. Adinarayana, and B. Jyothi, *AAPS PharmaSci Tech*, 6(03), 2005, 391-397
- [23]. R. Margesin, and F. Schinner, Bioremediation (Natural Attenuation and Biostimulation) of Diesel-Oil-Contaminated Soil in an Alpine Glacier Skiing Area, *Applied and Environmental Microbiology*, 67(7), 2001, 3127-3133.
- [24]. L. Charentanyarak, Heavy Metals Removal by Chemical Coagulation and Precipitation, *Water Science and Technology*, 39, 1999, 135-138.
- [25]. J. A. Dyer, N. C. Scrivner, and S. K. Dentel, A Practical Guide for Determining the Solubility of Metal Hydroxides and Oxides in Water, *Environ. Prog.* 171, 1998. 1–8.
- [26]. S. Moslem, R. Zohreh, I. Javid, M. Abbas, and R. Tahsin, Water Quality Assessment of the Zarivar Lake Using Physico-Chemical Parameters and NSF- WQI Indicator, Kurdistan Province-Iran, *International Journal of Advanced Biological and Biomedical Research*, 1(3), 2013, 302-312.
- [27]. W. Jianlong, Z. Xinmin, D. Decai, Z. J. Ding, Biosorption of Lead (II) from Aqueous Solution by Fungal Biomass of *Aspergillus Niger*. *Biotechnol.* 87, 2001, 273-277.
- [28]. L. Gianfreda, and M. A. Rao, Potential of Extra Cellular Enzymes in Remediation: A Review, *En: Yme Microb. Technol.*, 35, 2004, 339-354.
- [29]. P. D. Fuilbrook, "Kinetics." *Industrial Enzymology: The Application of Enzymes in Industry* (2nd Ed. T. Godfrey and J. Reichelt. Eds. Nature. New York, 1996).
- [30]. A. J. Russell, J. A. Berberich, G. F. Drevon, R. R. Koepsel, Biomaterials for Mediation of Chemical and Biological Warfare Agents, *Biomed Eng.*, 5, 2003, 1-27.
- [31]. A. Kandelbauer, O. Maute, R. W. Kessler, A. Erlacher, and G. M. Gubit, Study of Dye Decolourization in an Immobilized Lactase Enzyme-Reactor Using Online Spectroscopy, *Bioethanol Bioeng.*, 87(4), 2004, 552-563.
- [32]. Y. Liu, and Y. J. Liu, Biosorption Isotherms, Kinetics and Thermodynamics, *Sep. Purif. Technol.*, 61(3), 2008, 229–242.
- [33]. Omar, W.; Al-Itaw, H. *Amer. J. Appl. Sci.*, 2007. 4(7), 502-507

Akeem Adebayo Jimoh "Bioremediation Process of Effluent from Detergent and Food Industries in Jos, Nigeria: Kinetics and Thermodynamics" *International Journal of Engineering Science Invention (IJESI)*, vol. 07, no. 03, 2018, pp62-73