

Utilization Of Flexible Control Methods For D-Statcom In Mitigating Voltage Sags And Swells

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ABSTRACT:

This paper proposes three control strategies for D-STATCOM (Distribution Static Compensator) control system. The operation of these control techniques empowers D-STATCOM to moderate each sort of voltage contortions, insightfully (brought about by stack varieties and three-stage blame). This paper approves the execution of a D-STATCOM framework in enhancing conveyance framework execution under a wide range of framework related unsettling influences. The proposed framework is reenacted in PSCAD/EMTDC programming. Reproductions for the first and second strategies are executed and the aftereffects of reenactments for these two techniques are analyzed. At long last, the third strategy is proposed as a "Mixture Solution". The third technique includes all focal points of two specified strategies and mitigates every one of their disservices. The dependability and vigor of the control plots in the framework reaction to the voltage unsettling influences brought about by load varieties and three-stage deficiencies are clearly demonstrated in the reproduction comes about.

Key words: D-Statcom, Voltage Sags, Voltage Swells, Lookup Table, Energy Storage Systems.

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I. Introduction

Different strategies have been connected to lessen or mitigate voltage lists. The traditional techniques are by utilizing capacitor banks, presentation of new parallel feeders and by introducing uninterruptible power supplies (UPS). Notwithstanding, the power quality issues are not understood totally because of wild responsive power pay and high expenses of new feeders and UPS. The D-STATCOM has risen as a promising gadget to give, voltage hang alleviations as well as for a host for other power quality arrangements, for example, voltage adjustment, voltage swell moderation, glint concealment, control calculate rectification, and consonant control [1]. D-STATCOM is a shunt gadget that creates an adjusted three-stage voltage or current with capacity to control the extent and the stage edge [2].

For the most part, the D-STATCOM design comprises of a two-level VSC, a dc vitality stockpiling gadget; a coupling transformer associated in shunt with air conditioning framework, and related control circuits. The setups that are more advanced utilize multiples or potentially multilevel setups. Fig.1 demonstrates the schematic portrayal of the D-STATCOM. The VSC changes over the dc voltage over the capacity gadget into an arrangement of three-stage air conditioning yield voltages. These voltages are in stage and combined with the air conditioner arrangement of system through the reactance of the coupling transformer. Reasonable modification of the stage and size of the D-STATCOM yield voltages permits viable control of dynamic and responsive power trades between the D-STATCOM and air conditioning framework [3]. A control strategy in light of RMS voltage estimation has been exhibited in [4], [5] where they have been displayed a PWM based control conspire that requires RMS voltage estimations and no responsive power estimations are required. Additionally in this given strategy, Clark and Park changes are not required. However, they have examined voltage list/swell moderation because of simply the heap variety and utilizing a similar corresponding increase for a wide range of voltage bends while no three-stage flaws have been researched. This paper proposes three strategies for moderating the heap voltage lists and swells brought about by load varieties and three-stage deficiencies. In the primary method, the corresponding addition of the PI controller is kept up consistent and dc side arrangement in D-STATCOM is adjusted for relieving voltage mutilations. In the second technique, dc side topology of the D-STATCOM is unvaried and the relative pick up of the PI controller is altered by utilizing the proposed Lookup Table (that is arranged in view of bending sort) for alleviating voltage twists. The third strategy is a blend of focal points of two specified techniques. That is, both dc side topology of the D-STATCOM is adjusted and the corresponding addition of the PI controller is chosen wisely in view of the proposed Lookup Table. Impacts of load varieties furthermore, framework blames on the delicate burdens are researched and the control of voltage unsettling influences are examined and reproduced.

II. D-Statcom control base

This segment portrays the PWM-based control conspire with reference to the D-STATCOM. The point of the control plan is to keep up steady voltage size at the purpose of normal association (PCC), under framework unsettling influences. High exchanging frequencies can be utilized to enhance the productivity of the converter, without causing huge exchanging losses [4].

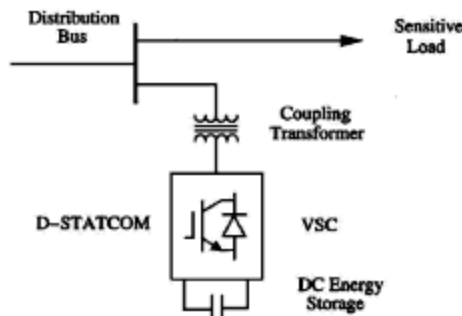


Fig.1. Schematic representation of the D-STATCOM

The piece graph of the control plot intended for the D-STATCOM is appeared in Fig. 2. It is construct just with respect to estimations of the voltage V_{rms} at the heap point.

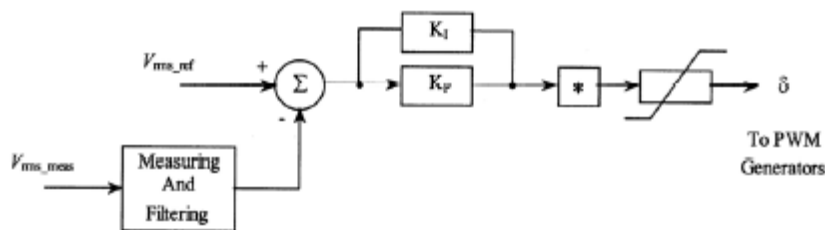


Fig.2. Control scheme designed for the D-STATCOM

The voltage blunder flag is acquired by contrasting the deliberate V_{rms} voltage and a reference voltage, V_{rms_ref} . A PI controller forms the distinction between these two flags with a specific end goal to acquire the stage edge δ that is required to drive the mistake to zero. The edge δ is utilized as a part of the PWM generator as the phase point of the sinusoidal control signal. The exchanging recurrence utilized as a part of the sinusoidal PWM generator is $f_{sw} = 1450$ (Hz) and the balance file is $M_a \approx 1$, [6]. The adjusting edge δ is connected to the PWM generators in stage A. The edges of stages B and C are moved 120 and 240 degrees, individually.

Fig. 3 demonstrates the schematic graph of the test framework used to do the transient displaying and investigation of the D-STATCOM. Two shifting burdens are associated with the 11 (kV), the optional side of the transformer. Brk.1 is utilized to control the time of operation of the D-STATCOM, and Brk.2 and Brk.3 control the association of Load 2 and Load 3 to the framework, separately. Furthermore, as Timed Fault Logic works, the three-stage blame happens. At the point when the Brk.2 is shut, the D-STATCOM supplies receptive energy to the framework, and when Brk.2 is opened and Brk.3 is shut, the DSTATCOM ingests responsive power keeping in mind the end goal to reestablish the RMS voltage to the reference value. When Brk.3 is opened and Timed Fault Logic works the D-STATCOM supplies receptive energy to the framework.

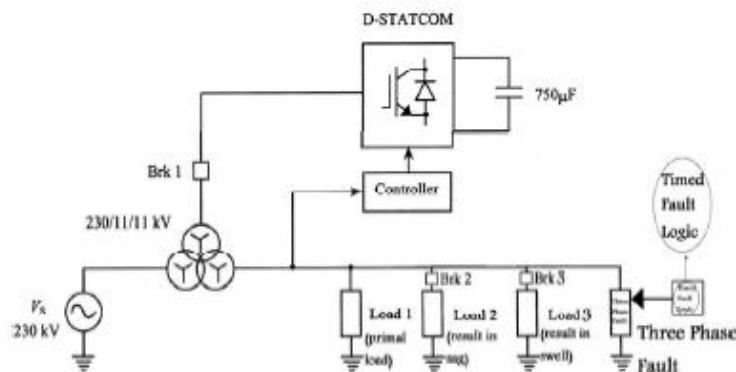


Fig.3. Schematic diagram of the test system used to carry out transient analysis of the D-STATCOM

III. Proposed control method

Corresponding increase is assuming an imperative part in PI controller in D-STATCOM. In the event that relative pick up is viewed as littler than an appropriate esteem, it causes a reduction in moderation and if corresponding increase is viewed as greater than a right esteem, it causes a swaying in RMS voltage profile and relief won't be great. For instance, in alleviation of droops and swells brought about by load varieties, the corresponding addition ought to be chosen rather little, and for relief of voltage drop created by three-stage blame, relative pick up ought to be chosen sufficiently huge. In this manner, relative increase must be chosen exact. Considering the way that each sort of voltage aggravation may occur in circulation frameworks, controller frameworks must be adaptable and have the capacity to relieve any sorts of load voltage contortions. With a specific end goal to relieve voltage twists brought on by three sorts of unsettling influences (voltage list and swell because of load varieties and voltage drop because of three stage deficiencies), three adaptable strategies are proposed as takes after:

3.1 First method

This strategy depends on coordinating D-STATCOM and Super-capacitor vitality stockpiling framework (ESS). In this method, the coordination and control of ESSs, for example, Super-capacitor, Ultra capacitor (UCAP) into a D-STATCOM is created to relieve such issues, upgrade control quality, and enhance dissemination framework unwavering quality. This technique builds up the control ideas of charging/releasing the UCAP by D-STATCOM and approves the execution of an incorporated D-STATCOM/UCAP framework for enhancing the conveyance framework execution under a wide range of framework related unsettling influences and three-stage flaws. Fig.4 demonstrates a commonplace circulation framework controlled by this strategy. A UCAP is incorporated with a dc capacitor. The UCAP capacitance is dictated by applying a consistent current release with $C = I \times dt/dv$. Since dv/di is practically consistent, UCAP capacitance can be displayed as a steady. The comparable arrangement resistance (ESR) is computed by measuring the yield voltage drop from no heap to consistent state load and after that isolating by the heap current. Since the open-circuit voltage has no critical impact on the ESR, the ESR can be displayed as a consistent [7]. The UCAP is displayed with 22.0(mF) capacitance and 320(m ω) ESR. Likewise in this strategy, the relative pick up of the PI controller is looked after consistent, which equivalent to 2420. Indeed, in this strategy, the dc side topology is fluctuated (by utilizing UCAP) and the relative pick up of the PI controller is kept steady in an improved esteem.

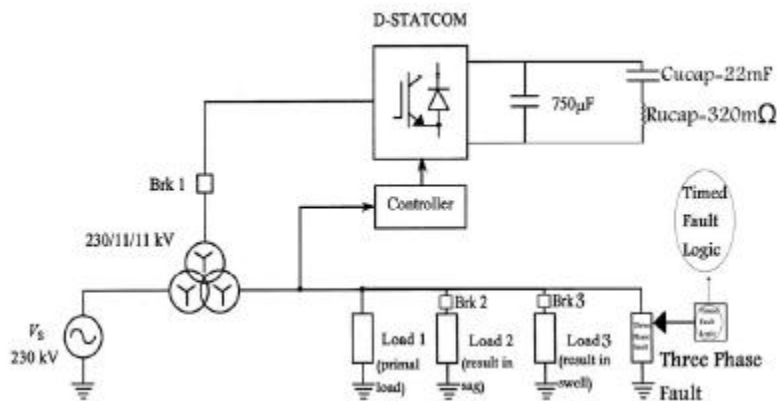


Fig.4. Distribution system with D-STATCOM integrated with UCAP and controller

3.2 Second method

This technique depends on utilizing the Look-up Table for deciding the reasonable relative pick up for each extraordinary voltage unsettling influence. Each PI controller has a corresponding addition that is assuming an essential part in D-STATCOM redress execution, and every voltage unsettling influence needs an extraordinary relative pick up for enhancing conveyance framework and D-STATCOM execution. In this way, it is important to utilize a different relative pick up for each sort of voltage unsettling influences. This strategy utilizes a Lookup Table for altering the relative pick up of the PI controller in D-STATCOM for moderating the voltage twists, insightfully.

As appeared in Fig. 5, stack current of one of the stages, (for example, stage An) is measured and its RMS esteem is calculated. Based on the heap current RMS esteem, the corresponding addition is resolved for every unsettling influence, formally.

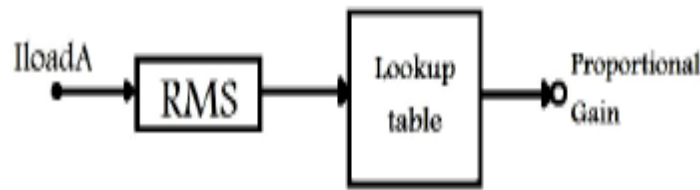


Fig.5.The application of Lookup Table for determining a suitable proportional gain

Each sort of the voltage unsettling influences stack current. In this strategy, a Look-up Table is masterminded in view of these heap current varieties as appeared in Table I.

TABLE I. LOOKUP TABLE ARRANGMENT FOR THE SECOND METHOD

RMS load current	0	7	10	12	20
Proportional gain	500	950	250	650	3750

In this Lookup Table, corresponding increases are resolved in view of Trial And Error and afterward the ideal esteem is chosen for every limit.

At whatever point the deliberate current RMS esteem at the heap point is arranged inside every limit, the related corresponding addition is separated from proposed Lookup Table. For example,when the heap current RMS esteem is in the vicinity of 7 and 10 the related corresponding increase is 950.

3.3 Third method

This strategy is a Hybrid arrangement and in light of joining of the first and second techniques. In this strategy, both of the Ultra-Capacitors and the Lookup Table are substantial. Truth be told, this strategy contains all points of interest of two said strategies what's more, dosage not involve any of their detriments. The speed of reaction and heartiness of the control plan are obviously appeared in the reenactment comes about.

IV. Simulation results

Fig. 3 demonstrates the test framework actualized in PSCAD/EMTDC to do recreations for the D-STATCOM. The test framework involves a 230(kV) transmission framework. A two-level D-STATCOM is associated with the tertiary twisting by shutting Brk.1 at 0.2 (s), for keeping up load RMS voltage at 1pu. A 750 (μF) capacitor on the dc side gives the D-STATCOM vitality stockpiling abilities. Recreations are completed for both situations where the D-STATCOM is associated with or disengaged from the framework. What's more, reenactments are completed for the first and second techniques and afterward they are analyzed together. At long last, the third strategy as Hybrid Solution of two as of now techniques is proposed.

The simulations relate to three main operating conditions:

1. In the period 0.5 – 0.8(s), the heap is expanded by shutting Brk. 2. For this situation, the voltage drops by just about 20% as for the reference esteem. At 0.8 (s), the Brk.2 is opened and stays all through whatever is left of the recreation.
2. In the period 1 – 1.3(s), Brk.3 is shut, associating a capacitor bank to the low voltage side of the system. The RMS voltage faces with 20% expansion regarding the reference voltage. At 1.3s, the Brk.3 is opened and remains all through whatever is left of the recreation.
3. In the period 1.5 – 1.8 (s), the three-stage blame is happened as Timed Fault Logic works. For this situation, the voltage drops by very nearly 13% concerning the reference esteem.

In this paper, the D-STATCOM by utilizing proposed control strategies mitigates a wide range of load point voltage twists.

Fig. 6 demonstrates the line voltages and the RMS voltage at the heap point for the situation when the framework works without D-STATCOM.

In $t = 0.2$ (s) D-STATCOM is associated with the circulation framework. The voltage twisting of the touchy load point is relieved utilizing the principal control technique, initially. In this strategy, relative pick up is consistent and equivalent to 2420 and a major UCAP (equivalent to 22 (mF)) is associated with the dc side of D-STATCOM.

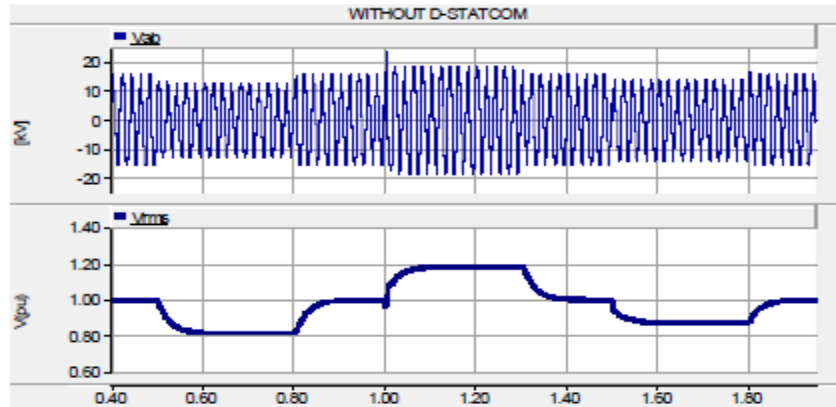


Fig.6. Line voltages and variation of RMS voltage (VRMS) at PCC without DSTATCOM

Fig. 7 demonstrates the remunerated line voltage(V_{ab}) at the heap point in interim 0.5 - 0.8 (s), (when the voltage drops by just about 20% on account of load increment by shutting Brk.2), and in interim 1 - 1.3 (s) (when the RMS voltage faces 20% expansion due to interfacing a capacitor bank to the low voltage side of the system by shutting Brk.3), and in interim 1.5 - 1.8 (s), (when the voltage drops by very nearly 13% in view of the three stage blame event by working Timed Fault Logic).

Fig.8 demonstrates the relieved RMS voltage utilizing first strategy where an extremely compelling voltage direction is given. It is watched that the main strategy has relieved voltage distortions(caused by load varieties and three-stage blame) genuinely well, in any case, relief time is fairly long in light of high time steady.

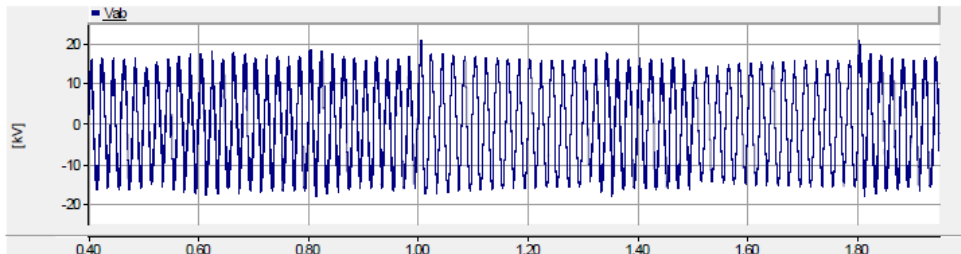


Fig.7. Compensated line voltage (V_{ab}) at the load point using first method

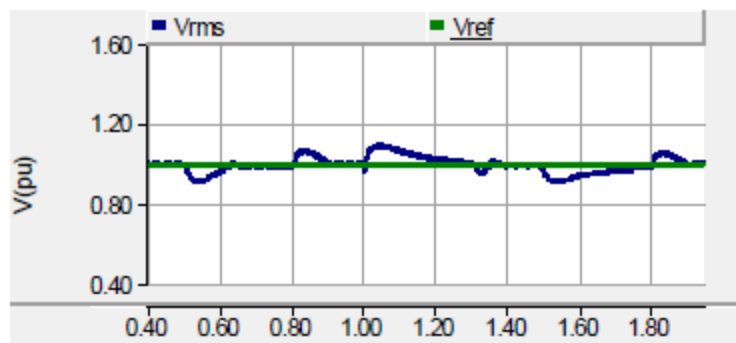
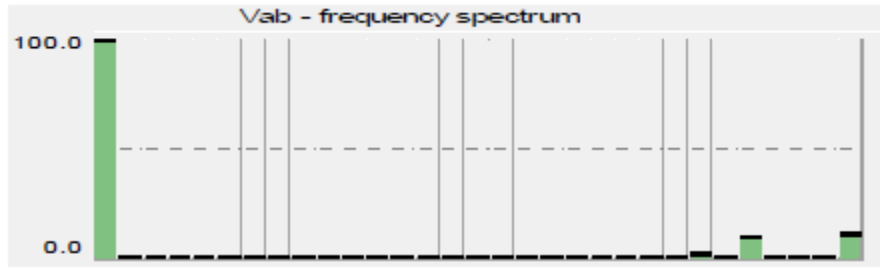
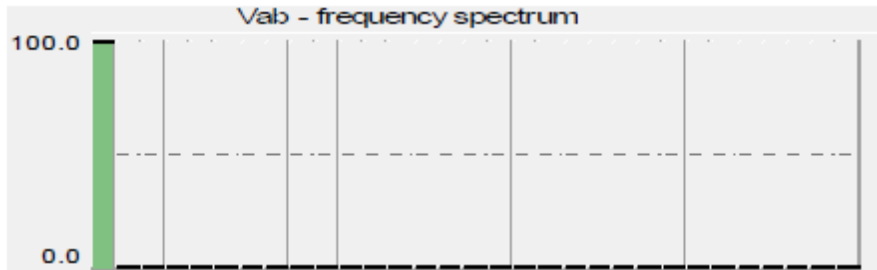


Fig.8. Mitigated RMS voltage using first control method

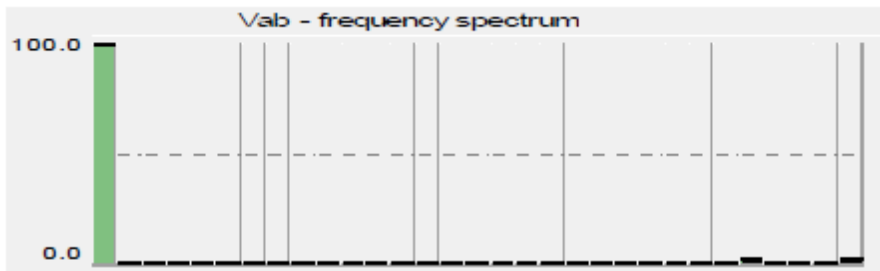
Fig. 9 demonstrates the V_{ab} (line voltage at the heap point) recurrence ranges amid moderation of hangs and swells that is displayed to percent. In Fig. 9, section (a) demonstrates the recurrence range for V_{ab} in interim 0.5 - 0.8(s), subsequent to wiping out transient states. It is seen, every even symphonious, and odd sounds up to 25th consonant are zero. Part (b) of these figures demonstrate similar graphs in interim 1 - 1.3 (s) that all sounds are zero and part (c) of these figures demonstrate the same outlines in interim 1.5 - 1.8 (s), it is watched that all music are relieved.



(a) Frequency spectrum for Vab in interval 0.5 – 0.8 (s)



(b) Frequency spectrum for Vab in interval 1 – 1.3 (s)



(c) Frequency spectrum for Vab in interval 1.5 – 1.8 (s)

Fig.9. Vab frequency spectrums during mitigation of sags and swells using first method

Additionally, the Total Harmonic Distortion (THD) for line voltage Vab amid the relief of droops and swells brought about by load varieties/three stage blame is displayed in Table II. It is watched that the THD for Vab in interims of blame event is near zero.

TABLE.II. VAB – THD FOR DURING OF MITIGATION USING FIRST METHOD

Disturbance intervals	0.5 – 0.8 s	1 – 1.3 s	1.5 – 1.8 s
THD	0.1467%	0.0025%	0.0136%

Fig.10 demonstrates the dc voltage of the VSC. Prior to the D-STATCOM begins working, the capacitor is charged to a consistent state voltage level of around 19 (kV). This underlying state of the capacitor enhances the reaction of the DSTATCOM furthermore, streamlines the necessities of the control framework. As appeared in Fig. 10, in the periods 0.5 – 0.8 (s) and 1.5– 1.8 (s), the D-STATCOM ingests dynamic power from the air conditioner framework to charge the capacitor and keep up the required dc connect voltage level.

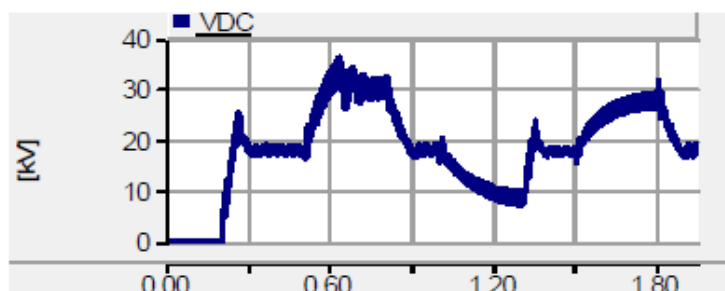


Fig.10. DC link voltage using first method

Presently, the touchy load point voltage is moderated utilizing the second control strategy. In this technique, the corresponding addition is removed from the Lookup Table orchestrated in Table I. Fig.11 demonstrates the repaid line voltage at the heap point amid alleviation of hangs and swells utilizing the second technique. Fig.12 demonstrates the relieved RMS voltage utilizing the second control strategy and Fig. 13 demonstrates the Vab recurrence ranges amid moderation of hangs and swells. The THD for the line voltage Vab amid alleviation of hangs and swells brought on by load varieties/three stage blame is displayed in Table III and the dc voltage of the VSC is appeared in Fig. 14.

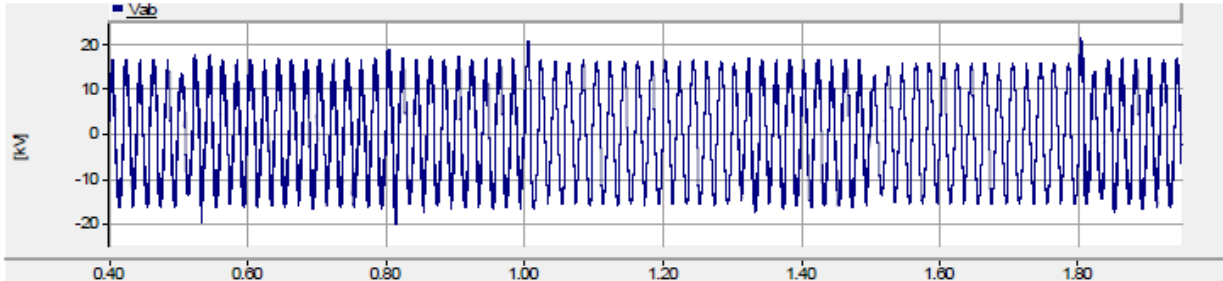


Fig.11. Compensated line voltage (Vab) at the load point using second method

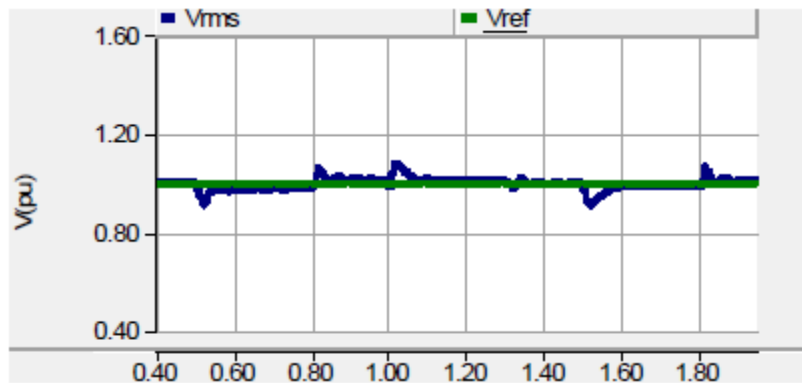
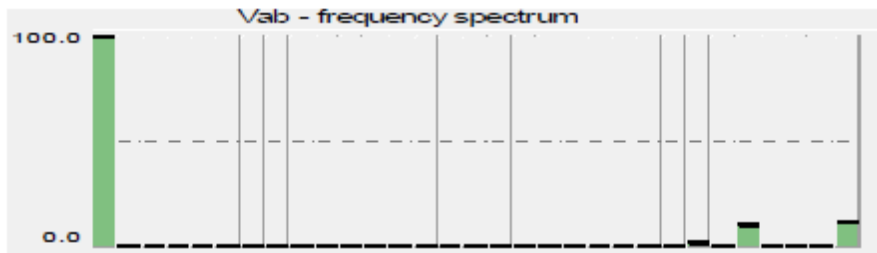
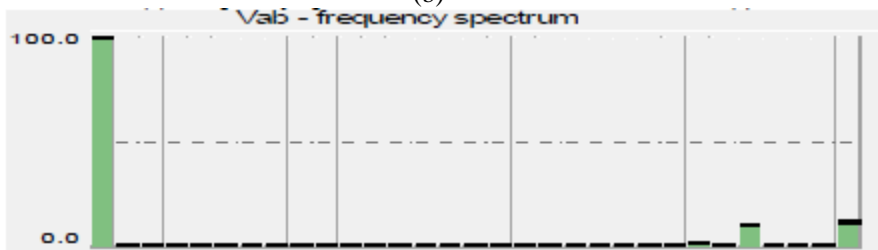


Fig.12. Mitigated RMS voltage using second control method

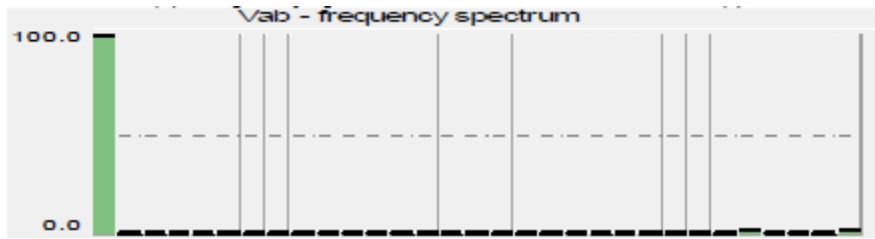


(a) Frequency spectrum for Vab in interval 0.5 - 0.8 (s)

(b)



(b) Frequency spectrum for Vab in interval 1 - 1.3 (s)



(c) Frequency spectrum for Vab in interval 1.5 - 1.8 (s)

Fig.13. Vab frequency spectrums during mitigation of sags and swells using second method

TABLE.III. VAB – THD FOR DURING OF MITIGATION USING SECOND METHOD

Disturbance intervals	0.5 – 0.8 s	1 – 1.3 s	1.5 – 1.8 s
THD	0.1472%	0.0049%	0.0150%

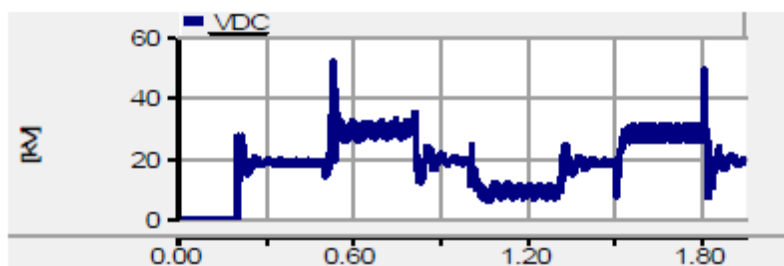


Fig.14. DC link voltage using second method

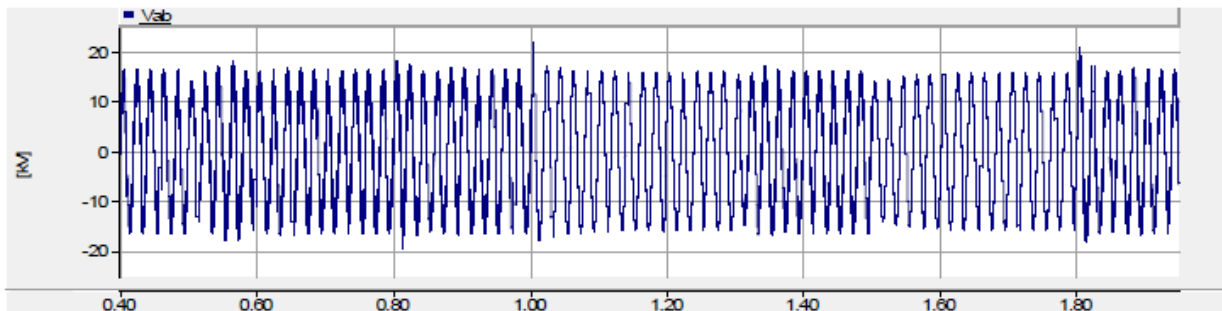


Fig.15. Compensated line voltages at the load point using third method

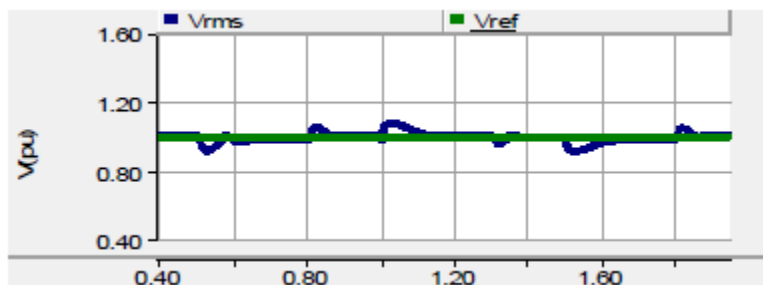
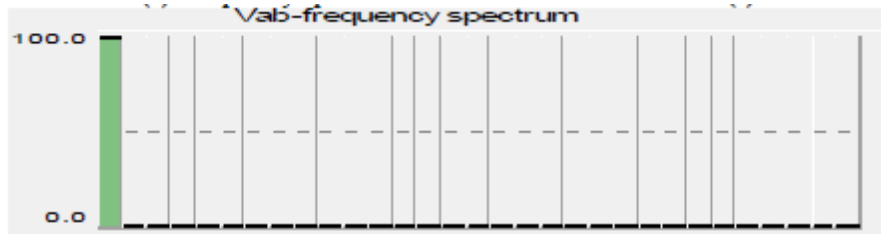


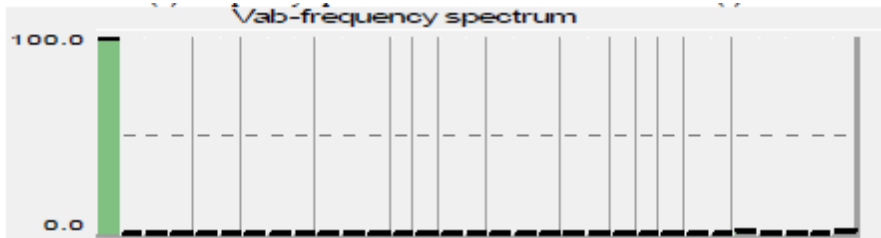
Fig.16. Mitigated RMS voltage using third method



(a) Frequency spectrum for Vab in interval 0.5 - 0.8 (s)



(b) Frequency spectrum for Vab in interval 1 - 1.3 (s)



(c) Frequency spectrum for Vab in interval 1.5 - 1.8 (s)

Fig.17. Vab frequency spectrums during mitigation of sags and swells using third method

TABLE.V. VAB – THD FOR DURING OF MITIGATION USING THIRD METHOD

Disturbance intervals	0.5 – 0.8 s	1 – 1.3 s	1.5 – 1.8 s
THD	0.1415%	0.0021%	0.0134%

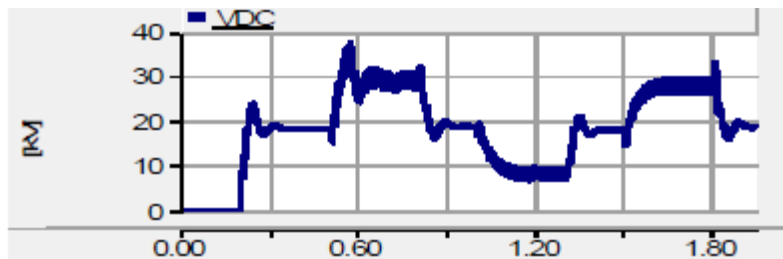


Fig.18. DC link voltage using third method

Proposed techniques focal points as for the great strategies are effortlessness and control accommodation and being adaptable, i.e. it can moderate voltage contortions brought about by both load varieties and three-stage blame just with the same control framework setting.

V. Conclusion

This paper has proposed three new control techniques for moderating the voltage mutilations, created by both load variety and three-stage blame, at the PCC. The primary technique was Integrating D-STATCOM and super-capacitor vitality stockpiling framework and the second strategy was Lookup Table application in deciding an appropriate relative pick up for each extraordinary voltage unsettling influence. At that point the reproduction consequences of two specified control strategies were looked at and their focal points/disservices were investigated. At long last, the third technique as a Hybrid Solution was suggested that not just contained favorable circumstances of two as of now said strategies additionally relieved their issues. Half breed control plan was tried under an extensive variety of working conditions, and it was watched that the third technique was exceptionally powerful and smart for each situation. This custom power controller may discover application in computerized enterprises with basic burdens.

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Biographies and Photographs

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V. Conclusion

This paper has proposed three new control strategies for alleviating the voltage twists, brought about by both load variety and three-stage blame, at the PCC. The main strategy was Integrating D-STATCOM and super-capacitor vitality stockpiling framework and the second technique was Lookup Table application in deciding a reasonable corresponding addition for each unique voltage unsettling influence. At that point the recreation aftereffects of two said control strategies were thought about and their preferences/drawbacks were broke down. At last, the third technique as a Hybrid Solution was suggested that not just involved points of interest of two as of now specified strategies additionally relieved their issues. Half breed control plan was tried under an extensive variety of working conditions, and it was watched that the third technique was exceptionally powerful and astute for each situation. This custom power controller may discover application in mechanized ventures with basic burdens.

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