Improved Reliability Analysis of Electricity Power Supply to Port Harcourt Distribution Network

¹S. L. Braide, 2E. O. kenneth

¹Department of Electrical/Computer EngineeringRivers State University, Port Harcourt, Rivers State Nigeria ²Faculty of Engineering Rivers State University, Port Harcourt, Rivers State Nigeria Corresponding auther: S. L. Braide

Abstract: This paper presents an analysis of reliability assessment for some area of electrical energy distribution system in Port Harcourt using analytical approach being supported by Electrical transient analyzer tool (ETAP) in order to run simulation on reliability assessment of the system. The investigation considered station-road, Amadi-North, floor-mail and Borikiri substation for purpose of analysis and verification. From the simulation results from system indices of ASAI: 0.9986pu, SAIFI: 0.7840 f/customer.yr, SAIDI: 12.66440hr/customer.yer, CAIDI: 16.128 hr/customer interruption in 2016 and ASAI: 0.9990pu, SAIFI: 0.78208/customer, yr. SAIDI:12.7740 hr/customer.yr, CAIDI: 16.108hr/customer interrupting in 2017. The reliability indices of the substations under study as obtained from the anlaysis, revealed that the reliability of the distribution system is below the set standard. Evidently improvement technique will be recommended in order to strengthen the activity of the system.

Keywords: reliability, distribution network, power supply, meantime to repair (MTTR), outage duration, *meantime to between failure (MTBF)*

Date of Submission: 20-06-2018

Date of acceptance: 06-07-2018 _____

Introduction I.

The reason for an electrical power system supply is for the provision of adequate supply of electrical power to all utilization point which also has to be at an economical rate for acceptance and reliability at reasonable level. Reliable power supply is of great importance in the electrical power system network for residential, commercial, industrial for purpose of economic growth for a given nation or place. Availability and reliability of a quality electric power supplied without interruption becomes extremely important. The importance of power system reliability is demonstrated when our electricity supply is disrupted, whether it decreases the comfort of our free time at home or causes the shutdown of our companies and results in huge economic deficits. The objective of Assessment of Power System Reliability is to contribute to the improvement of power system reliability [16].

Distribution of system reliability is an important measure of utility performance. In order to quantify the reliability of the distribution system, using system indices also known as reliability indices are used. The indices are statistical collections of reliability data. They are used as way to assess the effectiveness of the distribution system to supply power to the customer continually [2].

Amongst the three classof power system in Nigeria: Generation, Transmission and Distribution. Analysis and techniques of reliability and evaluation has shown the fact that the distribution network system at its level is less developed compared to generation and transmission, since it suffers lower outage than the others[4].

More so, based on analysis and statistics, it is known that the distribution power system accounts for 70% to 80% of the unavailability and reliability problems of the consumer, therefore, improving the distribution system is a vital step towards improving reliability and availability of electric power.

The fundamental purpose of Electrical power system is to provide an adequate electric power supply to all points of utilization at an economically acceptable rate with reasonable level of reliability.

Reliability of power supply has always been an important issue in the electric utility systems. Availability of high quality uninterrupted electric power system is essential to the industrial and economic growth of a nation.

Electricity supply involves a very complex and highly integrated system. Failures in any part of it can cause interruptions which range from inconveniencing a number of local residents, to major and widespread disruptions of supply. The economic impact of these outages is not restricted to loss of revenue by the utility or loss of energy utilization by the customer but include indirect costs imposed on the society and the environment due to the outage [11]

A power system consists of a generation, transmission and a distribution system. Traditionally, reliability analysis and evaluation techniques at the distribution level have been far less developed than at the generation or transmission levels since distribution outages are more localized and less costly than generation and transmission level outages.

However, analysis of the customer failure statistics of most utilities shows that the distribution system makes the greatest individual contribution to the unavailability of supply to a customer [10]. The distribution systems account for 80% of all customer reliability problems. Hence, improving distribution reliability is the major element required to improve customer reliability [11].

Since the primary purpose of the system is to satisfy customer requirements and the proper functioning and longevity of the system are essential requisites for continued satisfaction, it is necessary that both demand and supply considerations are appropriately viewed and included in the systems. Therefore, the distribution reliability is one of the most important in the electric power industry due to its high impact on the cost of electricity and its high correlation with customer satisfaction[6].

II. Problem Statement

Reliable electric power supply is essential for modern society as it is one of the vitalelementdriving every economy.

The rapid increase in the population of people migrating from the rural areas to the urban areas, particularly Port Harcourt, Rivers State has caused an unprecedented increase in energy demand. However, the power system facilities, particularly the distribution network has not experienced a proportionate expansion adequate enough for maintenance thus leading to:

- Overloading of the system,
- System losses due to mismatches between the power generation and power received.
- o unreliable power supply to consumers
- Transient behavior of the systems.
- Overloading of feeder (conductors, resulting to over-heating and insulation breakdown.
- Constant power outages leading to shutdown of production activities and eventual loss of revenue and gross profits.
- Overloading of substation
- Overloading of the system result to overheating of the system which has caused deficiency of the system to supply a reliable power to the consumer.

Therefore, there is a need to improve/upgrade and expand the distribution power system in Port Harcourt.

However considering the immense need for the improvement and the expansion of the distribution Network system in Port Harcourt will however not be achieved without a proper Reliability Assessment of the network.

Objectives of the Paper

- A reliability analysis of some substations from Port Harcourt Town distribution system shall be carried out using the Analytical Technique.
- To analyse the reliability indices of the distribution network of the area in view using performance data from Port Harcourt Electricity Distribution Company (PHEDC).
- To ascertain the Load Point Indices, System Indices and Cost Worth Indices of the distribution network which will thus reveal the reliability level of the network.

III. Materials And Methods

Materials

Electrical Transient Analyzer Program — ETAP

The Reliability Assessment software deployed to run the reliability assessment of the distribution network covered in this study is the Electrical Transient Analyzer Program (ETAP) software.

ETAP is a fully graphical electrical power system analysis program developed by Operation Technology Incorporated which has her headquarters in Irvine, California, USA. It is one of the most comprehensive tool for the design and analysis of power system reliability.

ETAP software capabilities and system analysis modules include but not limited toReliability Assessment Analysis, Load Flow Analysis, Short Circuit Analysis, OptimalPower Flow Analysis, Motor Acceleration Analysis, Transient Stability Analysis,Harmonics Analysis, Dc Load Flow Analysis, Dc Short Circuit Analysis, UnbalancedLoad Flow Analysis, Battery Discharge Sizing, Transformer MVA Sizing, Switching Sequence Management, etc. The reliability assessment module of ETAP can calculate and produce output reports of reliability indices like load point Indices (i.e., Failure rate of the distribution network, Average outage duration, and annual outage duration), system indices (i.e., System Average Interruption Frequency Index – SAIFI, System Average interruption Duration index – SAIDI, Customer. Average Interruption duration index – CAIDI and Average Service Availability Index – ASAI) and cost worth indices (i.e., Expected Energy Not Supplied – EENS, Expected InterruptionCost – ECOST, Average Energy Not Supplied – AENS etc.). Hence, it is in no doubtadequate, suitable and has the required capabilities needed for this study.

Methods

The Distribution Injection Substations covered in this study are fed from the Port Harcourt town 132/33kv injection transmission substation located at Nzirimo street by Port Harcourt - Aba express way, Port Harcourt which derives its power via two 132kv transmission lines from Afam power station locate at Afam, Oyigbo local government area of Rivers State.

The figure 1 illustrated in a tabular form as shown in table 1 below, AbonnemaWharf and Ikwerre Road 11kv outgoing feeders are supplied from Silver Bird 115MVA 33/11kv Injection Substation.Udi and Nsukka 11kv outgoing feeders and fed from Water Works 15MVA 33/11kv Injection Substation. State government secretariat 2xl5MVA 33/11kv Injection substation which is commonly referred to as Secretariat supplies Station Road, Amadi North, Flour Mill and Borokiri 11kv outgoing feeders.Ojoto, RSU, Federal and Wokoma 11kv outgoing feeders are fed from RSU 2xl5MVA 33/11kv Injection Substation which is domiciled at the Rivers State University, Nkpolu- Oroworukwor, Port Harcourt.

Finally, School of Nursing 15MVA 33/11kv Injection substation which is situated at the School of Nursing campus by Agip round-about, mile 4, Port Harcourt feeds Abacha Road, School of Nursing and Agip Road 11kv outgoing feeder.

	Table 1. Injection Substation/Techer Information and data										
S/ N	Injection Substation	Installed Capacity	Source	Station Outgoing Feeders	Voltage Level						
1.	Silver Bird 33/11ky	15MVA 33/11KV	PH Town	1. Abonnema	11kv						
	Injection Substation	100kva A T	132/33/11kv	Wharf	11kv						
	injeetion Substation	1001101111	TS Injection	2 Ikwerre							
			Substation	Road							
			Substation	Road							
2.	Water Works	15MVA	PH Town	1. Udi	11kv						
	33/11kv Injection	33/11KV	132/33/11kv TS	Nsukka	11kv						
	Substation	100kva	Injection								
		A.T	Substation								
3.		Substation	PH Town	1. Station Road	11kv						
		/ 200kva AT	132/33/llkv TS	2. Amadi North	11Kv						
			Injection	Flour Mill	11kv						
			Substation	Borokiri	11kv						
4.	RSUST 33/11kv	2×15MV A	PH Town	1. Ojota	11kv						
	Injection	33/11KV	132/33/11kv	2. UST	11kv						
	Substation	100kva A.T	TS Injection	Federal	11kv						
			Substation	4. Wokoma	11kv						
5.	School of Nursing	15MVA	PH Town	1. Abacha Road	11kv						
	133/11kv Injection	33/11KV	132/33/11kv	2. School of	11kv						
	Substation	100kva	TS Injection	Nursing							
		A.T	Substation	3. Agip Road	11kv						

Table 1: Injection Substation/Feeder Information and data

System Reliability

Every system is made up of component which determine and demonstrate the operations of the system weather it is working or not. This different components includes:

- i. Parallel system,
- ii. Series system. Etc.

The probability of the system to function adequately and properly the reliability is dependent on the type of system.

Parallel System

This type of system structure, the problem is that the rate of increase in reliability with an additional component decreases as number of component increases. "Law of diminishing returns" all the component must fail for the system to be down/stop functioning. Hence, overlapping outages is involved with failure modes of the load point. For the system to be interrupted, two or more components must be on outage state at the same time.





In this case the failure modes of the load point involve overlapping outages, That is, two or more components must be on outage at the same time in order to interrupt a load point as shown in figure 3. The equations used to evaluate the indices of the overlapping outage are given as:

• Average Failure rate of the system;

$$\lambda_p = \frac{\lambda_1 \lambda_2 (r_2 + r_2)}{1 + \lambda_1 r_1 + \lambda_2 r_2} = \lambda_2 \lambda_1 \lambda_2 (r_1 + r_2) \quad (1)$$

Where, $\lambda_1 r_1$ and $\lambda_2 r_2$ usually $\ll 1$

• Average Outage time of the system;

$$r_{p} = \frac{r_{1}r_{2}}{r_{1} + r_{2}} \tag{2}$$

Average Annual Outage time of the system;

$$\mu_p = \lambda_p r_p \tag{3}$$

Series System



Figure 4: Series structural system of the components.

This type of system has the problem that reliability decreases quickly as the number of components increases.

It is known that when one component is down the system is entirely down for all state and the system is in functional state when all the components are up, that all the component been up and in functional state, then the probability product of the series system been in upstate are equal. This component includes: - the transformer, lines (transmission/distribution), switches and breakers etc. are all consisted in the series system. All component must be in functional state for this type of system structure to be in upstate.

Similarly, a radial system consists of set of series components like; circuit breakers, lines, switches, transformers and "consumers". In the series structure both components must be intact for the purpose of system to function normally while in the parallel structure both must fail for the system to stop functioning. In this case, all the components are connected in series as shown in figure 4 and these equations are formulated as follows:

Average failure rate of the system;
$$\lambda_s = \lambda_1 \lambda_2 = \sum_{i=1}^{2} \lambda_i$$
 (4)

Average Outage time of the system; $r_s = \frac{\lambda_1 r_1 + \lambda_2 r_2 + \lambda_1 \lambda_2 + r_1 r_2}{\lambda_1 + \lambda_2} = \frac{\sum \lambda_i r_i}{\sum \lambda_i} = \frac{\mu_s}{\lambda_s}$ (5)

If $\lambda_1 \ \lambda_2 r_1 r_2 \ll \lambda_1 r_1 or \lambda_2 r_1 r_2$ Average Annual Outage time

$$\mu_s = f_s r_2 = \lambda_s . r_s \tag{7}$$

Where λ_i , is the failure rate at node i, r_i is the outage time at node i.

Reliability Indices

This is a necessary condition for having indices that expresses system failure event on probability and frequency basis. There are three basic indices: failure rate (λ) , outage duration (r) and average annual outage time (U), which permits the measurement of reliability at each load point to be quantified and allow subsidiary indices such as the customer interruption indices to be determined.

In a similar manner, distribution system is the segment of the overall system which links the bulk system to the individual customers. The distribution system reliability performance evaluation is normally concerned with the electric power supply adequacy to the customer/consumer load point.

The basic analysis of distribution system reliability indices are the three level load point indices: Average Failure Rate, (λ) , the Average Outage Duration, (r) and the Annual Outage Duration, (μ) .

Load Point Indices Analysis

In this analysis of the study case the radial system of the distribution, the reliability indices basic equation for analysis are presented :

(10)

Failure rate average;
$$\lambda = \sum \frac{F}{T} (f / yr)$$
 (8)

Load point repair rate;
$$\mu = \frac{To}{\left(\sum To / \sum F\right)} (repair / yr) (9)$$

Annual outage duration;
$$\mu\lambda = \sum To/T(Hr/Yr)$$

Outage duration average,

$$r_{y} = \frac{\mu_{y}}{\lambda_{y}} (Hr)$$
(11)

Mean time before failure,

$$\mathbf{MTBF} = \sum \frac{T}{F} \tag{12}$$

Mean Time to Repair,

$$MTTR = \sum \frac{T_o}{F}$$
(13)

Where, F – failure frequency of load point. T –Operating time (24hr \times 365 = 8760/hrs) T₀–Annual down time of load point

In the same manner, a radial system as it is the case in this paper, the basic equations for calculating the reliability indices at each load point, P are given as:

Average Failure Rate at load point,
$$p$$
,

$$\lambda_p = \frac{2L_F}{T} \left(f/yr \right) \tag{14}$$

where; F = Load point failure frequency $T = Operating Time (one year, i.e., 365 \times 24 hrs = 8,760 hrs)$ Annual Outage Duration at load point, p,

$$\lambda_{p} = \frac{\Sigma T dX}{T} \left(H r / yr \right) \tag{15}$$

Where;

 T_{dx} = Load point annual Down time (in hours) T = Operating Time Average Outage Duration at Load Point, p

$$r_p = \frac{\mu_p}{\lambda_p} (Hr) \tag{16}$$

Load Point Mean Time Before Failure,

$$MTBF = \sum \frac{T}{F} \tag{17}$$

Where; T = Operating Time and F = failure frequency Mean Time to Repair,

$$MTTR = \sum \frac{Tdx}{F}$$
(18)

Where,

Tdx = Load point annual Down time (in hours)

F = Load point failure frequency

System Indices

The system indices commonly used by electricity supply utilities are SAIFI, SAID1, CAIDI, ASAI AND ASUI. These indices can be calculated using the basic load point indices. That is, Average Failure Rate, (A), the Average Outage Duration, (r) and the Annual Outage Duration, (μ).

System Average Interruption Frequency Index, SAIFI is designed to give information about the average of sustained interruptions per customer over a predefined zone. Given as:

$$SAIFI = \frac{\sum_{\lambda P.NP}}{\sum Np} (f / cust - yr) (19)$$

Where;

 $\lambda_p = Failure rate$

Np = No of customers connected to load point, p

System Average Interruption Duration Index, SAIDI is commonly referred to as the customer minutes of interruption or customer hours. It is designed to give information about the average time the customers are interrupted.

$$SAIDI = \frac{\sum_{\mu p.Np}}{\sum Np} \left(Hr / cust - yr \right)$$
(20)

Where;

 $\mu_p \!\!=$ Annual Outage Duration at Load point, p

Np = No of customers connected to load point, p

Customer Average Interruption Index, CAIDI is the average time needed to restore service to the average customer per sustained interruption. Given as:

$$CAIDI = \frac{\Sigma \mu p.Np}{\Sigma \lambda p.Np} (hr / cust - Int.)$$
(21)

Average Service Availability Index,

$$ASAI = \frac{\Sigma N p.8,760 - \Sigma \mu p.N p}{\Sigma N p.8,760} (\%)$$
(22)

Where 8,760 is the operating time, (i.e., the No of hours in a calendar year, 365 ×24hrs)

COST WORTH INDICESExpected Energy Not Supplied, EENSEENS= Σ EENSp (MWh/yr)(23)EENSp= X_{p}, μ_{p} (24) X_{p} = average load of load point, p μ_{p} = annual outage duration at load point, pAverage Energy Not Supplied, AENSAENS = $\frac{\Sigma EENSP}{\Sigma Np} (mwhr/cust - yr)$ (25)Expected Interruption Cost, ECOSTECOST = Σ ECOST p (\$/yr)or (N/hr)(26)

Where;

ECOSTp = Expected Interruption Cost at load point, p $ECOSTp = Xp\Sigma f(rij)\lambda ej$ (27) Where:

 $X_p = Average Load of Load point, p$

F(rij) = SCDF = Sector Customer Damage Function

The steps associated with the method of reliability (Analytical Method) deployed in this study are summarized as thus;

- Calculate the load point indices of each load point being serviced by a given distribution system configuration considering all interruption events and system constraints contributing to its unavailability for each year of the system. That is, λ , μ , and \mathbf{r} .
- Calculate the system reliability indices using the calculated load point indices, load point average failure rate (λ_p) , Average Outage Duration (\mathbf{r}_p) and the Average Annual Outage Duration $(\boldsymbol{\mu}_p)$.

Repeat both steps for all load points of the distribution system configuration under study to obtain all system and cost worth indices; SAIFI, SAIDI, CA1DI, ASAI, EENS, ECOST etc.

	Table 2. Analysis and Calculations										
Load Point	Failure	Annual	Annual	No.of	Customer Type	Average	Peak				
	Freq.	Downtime(hrs)	Uptime(hrs)	Customer		Load(mw)	Load(mw)				
Station Rd	801	4413	3890	2120	Residential	3.9	4.8				
Amadi N.	440	4530	4230	1308	Res/Ind.	4.2	5.3				
Flour Mill	620	3881	4879	920	Comm./Res.	3.4	4.0				
Borokiri	890	5475	3285	2,770	Residential	4.3	5.5				

Table 2: Analysis and Calculations

The source of the historical data utilized in this study is the daily operational report/log book of the substations which are all under the management of Port Harcourt Electricity Distribution Company. The data collected was for a period of two years (2014 - 2015) and the historical data relevant to this study were properly analyzed and presented in a suitable form this study.

Some of the load point details extracted from the daily operational log book of the substations include;

- Record of Failure frequency on the network
- Record of Forced and scheduled Outages
- Record of the Duration Forced and Scheduled Outages
- Number of Customers Connected to each Load point
- The average load and peak load connected to each load point

Outage: Describes the state of a component or the system when it is not available to perform its intended function due to some event directly associated with the component or the system

Forced Outage: An outage caused by emergency condition directly associated with a component that requires the component to be taken out of service immediately, either automatically or as soon as switching operations can be performed.

Scheduled Outage: An outage that results when a component is deliberately taken out of service at a selected time, usually for the purpose of construction, preventive maintenance or repair. The key test to determine if an outage should be classified as forced or scheduled outage is as follows; if it is possible to defer the outage when such deferment is desirable, the outage is a scheduled outage otherwise, the outage is a forced outage.

Forced Outage Duration: It is the period from the initiation of an outage until the component is replaced or repaired.

Scheduled Outage Duration: It is the period from the initiation of the outage until construction, preventive maintenance or repairs are completed.

The substations historical data collected were on monthly basis but since the analysis in this study is annualized, the data were however cumulated and tabulated in an annualized form and classified mainly as thus;

Annual Outage Hours (Annual Downtime): The number of hours in a calendar year that the system was out of service by reason of forced or scheduled outage. This is a summation of the monthly downtime time hours.

Case 1: Station Road

Failure frequency, F = 791

Annual outage duration, is equivalent to down time = $\sum T dx = 4413$

Operating Time, $T = 365 \times 24$ hrs= 8,760

$$\mu_p = \frac{\sum T dx}{T}$$

$$\mu_p = \frac{4413}{8760} = 0.5037671$$

Meantime to repair;

$$MTTR = \sum \frac{Tdx}{F} = \frac{4413}{791} = 5.58 hrs$$

Applying the reliability equation, above we can determine our load point failure rate given as:

$$\lambda_p = \frac{\sum F}{T} = \frac{791}{8760} = 0.0902 f / yrs$$

Annual outage duration,

$$\mu_p = \frac{\sum T dx}{T} = \frac{4413}{8760} = 0.504 hrs / yrs$$

Average Outage Duration,

$$r_p = \frac{\mu p}{\lambda p} = \frac{0.504}{0.0902} = 5.59 hrs$$

Mean Time Before Failure (MTBF),

$$MTBF = \frac{T}{EF} = \frac{8760}{791} = 11.074589 hrs$$

Mean Time To Repair (MTTR), $MTTR = \frac{\sum Tdx}{F} = \frac{4413}{791} = 5.58hrs$

Similarly, we can effect the same equation and procedure to the other load point analysis

Case 2: Amadi North

 $\lambda_{p} = 0.0502 f / yr$ $\mu_{p} = 0.517 hrs / yrs$ $r_{p} = 10.30 hrs$ MTBF = 19.91 hrs MTTR = 10.29 hrs

Case 3: Flour Mill

```
\lambda_{\rm n} = 0.0708 f / yr
\mu_{p} = 0.4430 hrs / yr
r_{p} = 10.30 hrs
MTBF = 19.91hrs
MTTR = 10.29hrs
     = 6.28 hrs
rp
MTBF = 14.13hrs
MTTR = 10.29hrs
Borokiri;
λp
      = 0.0934 f/yr
      = 0.511 hrs/yr
μp
      = 5.47hrs
rp
MTBF = 10.71hrs
MTTR = 5.47 hrs
Other component failure rates are;
Transformer;
132/33kv = 0.002
33/11kv
           = 0.003
Circuit Breaker;
```

132kv	= 0.001
33kv	= 0.015
11kv	= 0.006
Bus Bar	;
132kv	= 0.001
33 kv	= 0.001
11kv	= 0.015

Table 3:Shows the total load point indices of the system case

		1 7	
Load Point	$\lambda_{\rm T}({\rm f/hr})$	r _T (hours)	$\mu_{\rm T}({\rm hr/yr})$
Station Rd -Lpl	0.8787	9.29	8.1661
Amadi N. –Lp2	0.8387	9.70	8.1391
Flour Mill –Lp3	0.8593	9.38	8.0631
Borokiri-Lp4	0.8900	9.14	8.1325

System Indices

The system indices of the system case are calculated using equation (19), (20), (21) and (22). Applying these equations yields;

System Average Interruption Frequency Index,

 $SAIFI = \frac{\sum \lambda p.Np}{m} =$ $\sum Np$

 $\{(0.8787 \times 2,120) + (0.8387 \times 1,308) + (0.8593 \times 920) + (0.8900 \times 2,770) + \}$

2,120 + 1,308 + 920 + 2,770SAIFI = 0.873f/cust-yr.

System Average Interruption Duration Index,

 $SAIDI = \frac{\sum \mu p.Np}{\sum \mu p.Np} =$ $\sum Np$

 $\{(8.166 \times 2,120) + (8.139 \times 1,308) + (8.063 \times 920) + (8.132 \times 2,770) + \}$ 2,120 + 1,308 + 920 + 2,770

SAIDI = 8.134hrs/cust-yr.

Customer Average Interruption Index, CAIDI

 $CAIDI = \frac{\sum \mu p.Np}{\sum \lambda p.Np} =$

 $\{(8.166 \times 2,120) + (8.139 \times 1,308) + (8.063 \times 920) + (8.132 \times 2,770) + \}$ $\{(0.8787 \times 2,120) + (0.8387 \times 1,308) + (0.8593 \times 920) + (0.8900 \times 2,770)\}$

CAIDI = 9.317hrs/cust-lnt.

Average Service Availability Index, $\Sigma Nn \otimes 760 - \Sigma IIn.Np$

$$ASAI = \frac{\sum Np.8,760 - \sum \mu p.Np}{\sum Np.8,760}$$

$$\sum Np.8,760$$

ASAI = $\underline{(7,1186\times8,760) + (8.166\times2,120) + (8.139\times1,308) + (8.063\times920) + (8.132\times2,770)} ASAI = 0.99901\times100$ 7,118×8,760

ASAI = 99.91%

Table 4:Shows the system indices for the sample system

Index	Values	Unit
SAIFI	0.873	Int./yr
SAIDI	8.134	Hrs/yr
CAIDI	9.137	Hrs/cust-int.
ASAI	99.91	%

Cost Worth Indices

The cost worth indices of the system case are calculated using equations (28) to (29) as follows; $EENS = \Sigma EENSp (mwh/yr)$ (28) $EENSp = Xp.\mu p$ (29)Where; Xp = average load of load point, p μp = annual outage duration at load point, p **Expected Energy Not Supplied, EENS** EENS = { $(3.9 \times 8.166) + (4.2 \times 8.139) + (3.2 \times 8.063) + (4.3 \times 8.132)$ }

EENS = 128.41 mwh/yr Expected Interruption Cost, ECOST $ECOST = \Sigma ECOSTp$ = 70,598.46 + 256,913.30 + 318,183 +77,128.95 ECOST = \$722,823.71 (for N250 for \$1 = N180,705,927.5

Load Point	EENSp (mwh/Cust-Yr)	ECOSTp (\$/Yr)	AENS							
Station Rd - 1	31.8478	70,598,46	0.015							
Amadi N2	34.1841	256,913.30	0.026							
Flour Mill -3	27.4145	318,183.00	0.029							
Borokiri-4	34.9699	77,128.95	0.013							
TOTAL :	128.413	722,823.71	0.018							

Table 5: Shows the cost worth indices of the system case.



Figure 1: Distribution feeders: station road, Amadi north, floor mail and Borikiri (before simulation)



Figure 2: Distribution feeders: station road, Amadi north, floor mail and Borikiri (after simulation)

			Com	neetions)		
ETAP 12.6.0 - [OLV1 (Reliability Assessme	etil ETAP Report	- Untitled / Branch Connections	-			- 0 ×
File Edit View Project Library R	ules Dela File View He	leip				_ 8 ×
D 💕 🖬 🖨 🔍 🖄 🐘 🧑 🍳	AR BOK	4 P H 1/1 M	G m 1251 - Q		a star	
Base • 🔂 OLV1						
💶 😂 🌮 🔨 🗛						
		B	anch Connections			
Ta						- 0 -
		CKT/Branch	Ces	nected Bus ID		0
<u>=</u>		ID Type	From Bas	To Day		
	TI	2W XPMR	Port Hast ourt Town	port Marcourt		
	72	2 W XPMR	Port Hast ours Town	port Marcourt		1.64
	73	2W XPMR	Sec	Sec.		1.1.1
-	T4	2 W 209MR	Sec	Sec.		63
and the second s						10.
1						
						22
0						-
102						
128						
+0						
75						
90						
58						
•						

	_					
10						
X 69 Y 81						Base
	0.0	w 8				7-33 AM
			8			4/28/2018

 Table 6: Result of Distribution feeders: Station road, Amadi north, floor mail and Borikiri (Branch Connections)

Table 7: Result of Distribution feeders: Station road, Amadi north, floor mail and Borikiri (Branch Input Data)

EJ File Edit View Project Library Rules D	File View Help				_	_	_				_ / # ×
	3 3 X 4 5 8	1 /1	x 5 m 125%	. 0					Bustress Oldert		
Rate • Children OLVI	(_		
										1	
	Project: Location					ETAP 12.6.0H			Page: 1 Date: 28-04		0 0 0 0 0 0
(e (a)	Contract								SN: Parision Bass		(T)
<i>a</i>	Filmame	sen project			Stu	idy Case: 1	R.A.		Config Norma		67.4
/											(C)1
0											22
	-				- 400 - 400						
					Branch	h Input D	ata				
+8							Repla	cement			
CTI I		Transformer	24	λp	MTTR	Time	Avail.	Time			
90		10	Type f/yv	t/yr	haser	Losr	Tes No	hour			
0	TI	3W 3	CFM.R. 0.0150	0.0000	200.00	200.00	25.0	10.00			
	12	2003	CPAIR 0.0150	0.0000	200.00	200.00	No	10.00			
	т4	2W 3	CFM.R. 0.0150	0.0000	200.00	200.00	No	10.00			
	2257							Subreport Branch rpt			
								Loss of Contract o			
											-
											,
A144 T122		017		-			_		-		Dase 734 AM
			ý ý								4/28/2018

Table 8: Result of Distribution feeders: Station road, Amadi north, floor mail and Borikiri (Bus Input Data) data



			Electrical Transien	Analyzer Program		<u> </u>
1			Reliability	Analysis		
		Load	ding Category (1):	Design		
		Load	d Diversity Factor:	None		
		Iotal				
	Number of Buses:	4				
		XFMR2 XFMR3	Reactor Line/Cable	Impedance Tie PD	SPDT	
	Number of Branches:	4 0	0 0	0 1	0	
		Synchronous Power				
		Generator Grid	Inverter Total			
	Number of Sources	0 1	0 1			
		Synchronous Induction. Motor Machine	Static Lumped Load Load	Total		
		<u> </u>				
	Number of Loads:	0 0	0 4	•		
	System Frequency:	50 Hz				
	Unit System:	English				-
	Project Filename:	sep project			-	

Table 9: Result of Distribution feeders: Station road, Amadi north, floor mail and Borikiri (Reliability Analysis)

 Table 10: Result of Distribution feeders: Station road, Amadi north, floor mail and Borikiri (Reliability Analysis)

ETAP Report - Untitled / Cover				-	, <i>,</i>				and the second		- ×
File View Help											
	125% 💌 🍘									Busines	Objects
			Electi	ical Transien	t Analyzer Pr	ogram					
				Reliability	Analysis						
			Loading Cat	ng ory (1):	Design						
			Load Divers	tyFactor:	None						
		T									
		1001									
	Number of Buses:	4									
		XFMR2 3	XFMR3 Reacto	r Line/Cable	Impedance	Tie PD	SPDT	Total			
	Number of Branches:	4	0 0	0	0	1	0	5			
		for the second	2								
		Generator	Grid Inverte	r Total							
			1 0								
	Number of sources:	0	1 0	1							
		Synchronous I	Induction Static	Lumped	Tent						
			subreport:Cove	nka.nptp.oao	1044						
	Number of Loads:	0	0 0	4	4						
	System Frequency:	50 Hz									
	Unit's ystem: Project Filanama	Engusa	et								
	Output Filename:	C:ETAP	1260 sep project U	ntitled.RA1							
											-
	😂 🚯 🕅	V 2	*							· 🐚 🕯 🐠 7135	AM
										4/28	2016

Table 11: Result of Distribution feeders: Station road, Amadi north, floor mail and Borikiri (Load Input Data)





ETAP 12.6.0 - [OLV1 (Reliability Assessment)]		and the second second	_	_	_							- 0 ×
File Edit View Project Library Rules Defaults	Tools RevControl Res	al-Time Window Help		le l		-8						_ // ×
			M 157 69 E	TAP (Default)		10.110	Ind					
				• Unkbed	• [10/2] LO	ad Point Nepo						
			1								L Interior N	
1770	TAP Report - Ur	ntitled / Load Point Report	1.00	-								i Po
123	File View Help											0 -
L & L	🕞 🍊 H 4	▶ H 1 /1	🛛 🖾 🕅 12	5% 💌 🕜							Business Objects	
					Average	Average	Annual				· · ·	R
			Bus		Rate	Duration	Duration	EENS	ECOST	IEAR		- <u>1001</u>
		ID	Load Sector	Connected Bus ID	f/yr	hear	hr/yr	MW hr / yr	\$ / yr	\$ / kW hr		
		port Marcourt	N/A		0.6675	3.62	2.4150	0.0000	0.00	0.000		S.
		Port Hamourt Town	N/A		0.6575	2.99	1.9630	0.0000	0.00	0.000		
A		Sec	N/A		0.7840	16.13	12.6440	0.0000.0	0.00	0.000		10°5
		Sec.	N/A		0.7840	16.13	12.6440	212.2612	0.00	0.000		2-1
		station road	None	Sec.	0.7840	16.13	12.6440	52.3936	0.00	0.000		
12003		Amadi north	None	Sec.	0.7840	16.13	12.6440	56,4239	0.00	0.000		
		Floor mail	None	Sec.	0.7840	16.13	12.6440	45.6765	0.00	0.000		
<u>+</u>		Borikiri	None	Sec.	0.7840	16.13	12.6440	57.7673	0.00	0.000		
-6		Afam power	None	Port Harcour Subreport:Loa	dReport.rpt d0	2.22	1.4360	0.0000	00.0	0.000		
Liti I												
53												
U												
-	1											

•												
× 🗆					_	_	_	_	_	_		
X: 137 Y: 33												Base
) 🔍 🛃	W 2	- 2								- 18	1:45 AM
x:137 Yi 33	. 🤹 🌜	· · · · · · · · · · · · · · · · · · ·	\$								- N	Base 7:45 AM 4/28/2018

 Table 13: Result of distribution feeders: Station road, Amadi north, floor mail and Borikiri (Sector Interruption





	File View Help			
	🔐 🍊 Н Ч Р Н 🚺 /1 -	😹 🕉 🕅 125% 💌 🥝	Business Objects	
🚰 Base 👻 🔁 OLVI 👻 🔝 OL	Project:	LIME	Page: A	
	Location	12.6.010	Date:	
	Contract		8N-	A
77.	Contract.		Bardeland and	
128	Angineer	Study Case: RA	Revision:	
- 3 -	Filename: sep project		Config.:	
N. Contraction of the second sec	1			Line Line Line Line Line Line Line Line
				1.44
	1			
	1	SUMMARY		
	1			\$0 ₃₀
A	1	System Indexes		
	1			
	1	S/GP1 0.7840 17 customer.yr		
14 ME	1	SAIDI 12.6440 hr/ customer.w		
1222	1			
<u>4.5</u>	1	CAIDI 16.128 hr / customer interruption		
<u>TV</u>	1			
E I	1	AS AI 0.9986 pu		
90	1	ATT 0.00114		
	1	Subranart Summary mt		
	1	EEN8 212.261 MW br / yr		
	1			
	1	ECOST 0.00 \$ / 3#		
•		AENS 53.0653 MW hr / customer.yr		
····		TEAR 0.000 \$ / kW br		
	1			
	1			
	1			
	1			
	1			
	1			
	1			
<				
X: 150 Y: 134				Base
	🕒 🔍 🛃 🙀 🤶	*		 Image: Apple of the second seco
				4/28/2018

Conclusion

IV. Conclusion And Recommendation

The reliability assessment for substations for some Port Harcourt town distribution network are presented using analytical approach and being supported by ETAP simulation tool.

The result presented in the study case using the reliability system indices: SAIFI, SAIDI, CAIDI, ASAI etc, this shows quantitatively that the entire system is below or declared international set standards, hence the system behaviour is unreliable. Essentially, improving techniques configuration will be recommended for purpose of improving system stability.

Recommendation

Considering the analysis of this study case, the following recommendation for purpose of improving the system reliability of the distribution networkarestated:

- i. Expansion of the network by the electric utilities: PHEDC, etc in order to take care of the overload problem on the system.
- ii. System reconfiguration is considered in order to reduce the number of customer connected to already over stressed distribution network.
- iii. Immediate replacement of faulty or aged system component with quality or new ones.

References

- [1]. PHEDC, (2014 and 2015), 'Daily Dispatching and Operational Logbooks' of Secretariat, Silver Bird, Water Works, U.S.T., and School of Nursing injectionsubstations, Port Harcourt, Rivers State-Nigeria.
- [2]. Venu B, Bhargava C. and Sumanth K., (2014), 'Reliability Assessment of Radial Distribution System by Using Analytical Methods', International Journal of Engineering Studies, vol.4(4), pp!85-196.
- [3]. Harikrishna K., Ashok V, Chandraskhar P, Raghnatha T and Deshpande R., (2013) 'Predictive Reliability in the Power Distribution System', the Journal of CPRL, vol.9(3)_f pp335-342.
- [4]. Obaro B.A, (2010), 'Reliability Evaluation of Distribution Systems Using Failure Modes, Effect & Analysis', Master's Thesis, University of Port Harcourt.
- [5]. Tempa D., (2009), 'Reliability Assessment of Distribution Systems a case study on Wangdue Distribution System in Bhutan', Masters Dissertation, Norwegian University of Science and Technology.
- [6]. Hag-Kwen Kim, (2009) 'Reliability Modeling and Evaluation in Aging Power Systems', Masters Dissertation, A&M University.
- [7]. Ogujor E.A. and Kuale P.A. (2007), 'Using Reliability Indices-Markov Model in Electric Power Distribution System', International Journal of Electrical and Power Engineering 1(4), pp416-420.
- [8]. Akhikpemelo A. (2011), 'Reliability assessment of electrical distribution in Port Harcourt Area', Master's Thesis, University of Port Harcourt.
- [9]. Phil P.B. and Robert W.D.M, (2000), 'Determining the Impact of Distributed Generation of Power, Part 1 Radial Distribution Systems', Power Engineering Society Summer Meeting, IEEE, vol.3 pp. 1645-1656.
- [10]. Billinton R., Cui L, Pan Z. and Wang P., (2002) 'Probability DistributionDevelopment in Distribution System Reliability Evaluation', Electric Power Components and Systems, vol.30; pp907-916.
- [11]. Billinton R., Leite da Silva A. M., Cassula A. M., and Manso L. A. F., (2002) 'Integrated Reliability Evaluation of Generation, Transmission and Distribution Systems', Generation, Transmission and Distribution, IEE Proceedings-, vol. 149, pp. 1-6.
- [12]. Fang Y., Sun W.K and George S., (2005) 'Comprehensive power system reliability assessment', Final project, Georgia Institute of Technology.
- [13]. Hegazy V. G., Salama M: M. A., and Chikhani A. Y., (2003) 'Adequacy Assessment of Distributed Generation Systems Using Monte Carlo Simulation'.
- [14]. Robert P. Broadwater, Hesham E. Shaalan, (1994) 'Distribution System Reliability and Restoration Analysis', Electric Power System Research, 29 pp. 203-211.
- [15]. Rotwell J. (2004), 'The Reliability Triangle, Transmission & Distribution World", pp. 54-56.
- [16]. Violentis, J.B, Platis A.N, Grawanis G.A, Koutras V.P. (2001) 'Electrical Substation Efficient Maintenance Policies Based On Semi-Markov Modeling and Approximate Inverse Preconditioning', Department of Electrical and Computer Engineering, Democritus University of Thrace, 12, Vas. Sofias Street, GR 67100 Xanthi, Greece.
- [17]. Wei Zhang, (1998) 'Reliability Evaluation of Bulk Power Systems using Analytical and Equivalent Approaches', Doctoral Dissertation, University of Saskatchewan
- [18]. IEEE, (2011), 'Guide for Power Distribution Reliability Indices', IEEE std 1366, 2011 edition

S. L. Braide "Improved Reliability Analysis of Electricity Power Supply to Port Harcourt Distribution Network "International Journal of Engineering Science Invention (IJESI), vol. 07, no. 07, 2018, pp 23-36